

DIETZGEN
TRADE MARK

ENGINEERS'
LEVEL BOOK

No. 410

Maybe NW

Co. Chester 26.90

Tray

mail

sliding

wood hub. ironed knives in

Lake Co

Geauga Co.

mail. in maple tree 54.21

536.30

Brail

in 10 maple. 33.24

179.36

mail in

15 Maple

33.24

1936



EUGENE DIETZGEN CO.

DRAWING MATERIALS, MATHEMATICAL and
SURVEYING INSTRUMENTS

Chicago New York San Francisco New Orleans Pittsburg Toronto

Distances from Center of Roadway for Cross-Sectioning
Roadway 16 feet wide. Side Slopes 1 on 1.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.1	8.2	8.3	8.4	8.5	8.6	8.7	8.8	8.9	0
1	9.0	9.1	9.2	9.3	9.4	9.5	9.6	9.7	9.8	9.9	1
2	10.0	10.1	10.2	10.3	10.4	10.5	10.6	10.7	10.8	10.9	2
3	11.0	11.1	11.2	11.3	11.4	11.5	11.6	11.7	11.8	11.9	3
4	12.0	12.1	12.2	12.3	12.4	12.5	12.6	12.7	12.8	12.9	4
5	13.0	13.1	13.2	13.3	13.4	13.5	13.6	13.7	13.8	13.9	5
6	14.0	14.1	14.2	14.3	14.4	14.5	14.6	14.7	14.8	14.9	6
7	15.0	15.1	15.2	15.3	15.4	15.5	15.6	15.7	15.8	15.9	7
8	16.0	16.1	16.2	16.3	16.4	16.5	16.6	16.7	16.8	16.9	8
9	17.0	17.1	17.2	17.3	17.4	17.5	17.6	17.7	17.8	17.9	9
10	18.0	18.1	18.2	18.3	18.4	18.5	18.6	18.7	18.8	18.9	10
11	19.0	19.1	19.2	19.3	19.4	19.5	19.6	19.7	19.8	19.9	11
12	20.0	20.1	20.2	20.3	20.4	20.5	20.6	20.7	20.8	20.9	12
13	21.0	21.1	21.2	21.3	21.4	21.5	21.6	21.7	21.8	21.9	13
14	22.0	22.1	22.2	22.3	22.4	22.5	22.6	22.7	22.8	22.9	14
15	23.0	23.1	23.2	23.3	23.4	23.5	23.6	23.7	23.8	23.9	15
16	24.0	24.1	24.2	24.3	24.4	24.5	24.6	24.7	24.8	24.9	16
17	25.0	25.1	25.2	25.3	25.4	25.5	25.6	25.7	25.8	25.9	17
18	26.0	26.1	26.2	26.3	26.4	26.5	26.6	26.7	26.8	26.9	18
19	27.0	27.1	27.2	27.3	27.4	27.5	27.6	27.7	27.8	27.9	19
20	28.0	28.1	28.2	28.3	28.4	28.5	28.6	28.7	28.8	28.9	20
21	29.0	29.1	29.2	29.3	29.4	29.5	29.6	29.7	29.8	29.9	21
22	30.0	30.1	30.2	30.3	30.4	30.5	30.6	30.7	30.8	30.9	22
23	31.0	31.1	31.2	31.3	31.4	31.5	31.6	31.7	31.8	31.9	23
24	32.0	32.1	32.2	32.3	32.4	32.5	32.6	32.7	32.8	32.9	24
25	33.0	33.1	33.2	33.3	33.4	33.5	33.6	33.7	33.8	33.9	25
26	34.0	34.1	34.2	34.3	34.4	34.5	34.6	34.7	34.8	34.9	26
27	35.0	35.1	35.2	35.3	35.4	35.5	35.6	35.7	35.8	35.9	27
28	36.0	36.1	36.2	36.3	36.4	36.5	36.6	36.7	36.8	36.9	28
29	37.0	37.1	37.2	37.3	37.4	37.5	37.6	37.7	37.8	37.9	29
30	38.0	38.1	38.2	38.3	38.4	38.5	38.6	38.7	38.8	38.9	30
31	39.0	39.1	39.2	39.3	39.4	39.5	39.6	39.7	39.8	39.9	31
32	40.0	40.1	40.2	40.3	40.4	40.5	40.6	40.7	40.8	40.9	32
33	41.0	41.1	41.2	41.3	41.4	41.5	41.6	41.7	41.8	41.9	33
34	42.0	42.1	42.2	42.3	42.4	42.5	42.6	42.7	42.8	42.9	34
35	43.0	43.1	43.2	43.3	43.4	43.5	43.6	43.7	43.8	43.9	35
36	44.0	44.1	44.2	44.3	44.4	44.5	44.6	44.7	44.8	44.9	36
37	45.0	45.1	45.2	45.3	45.4	45.5	45.6	45.7	45.8	45.9	37
38	46.0	46.1	46.2	46.3	46.4	46.5	46.6	46.7	46.8	46.9	38
39	47.0	47.1	47.2	47.3	47.4	47.5	47.6	47.7	47.8	47.9	39
40	48.0	48.1	48.2	48.3	48.4	48.5	48.6	48.7	48.8	48.9	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 30.6. For same slopes but other widths of roadbed, correct above figures by one-half difference in width of roadbed; thus in example above, for 20 ft. roadbed distance will be $30.6 + (20 - 16) \div 2$ or 2 ft. added to $30.6 = 32.6$. For slopes of 1 on 1½ see inside of back cover.

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140A

Please Return to

F. R. Zethmayr

Chardon, O.

98

phone 327

Bottles, Cottrell
Subdivisions
Chester X Roads

See over
for Index

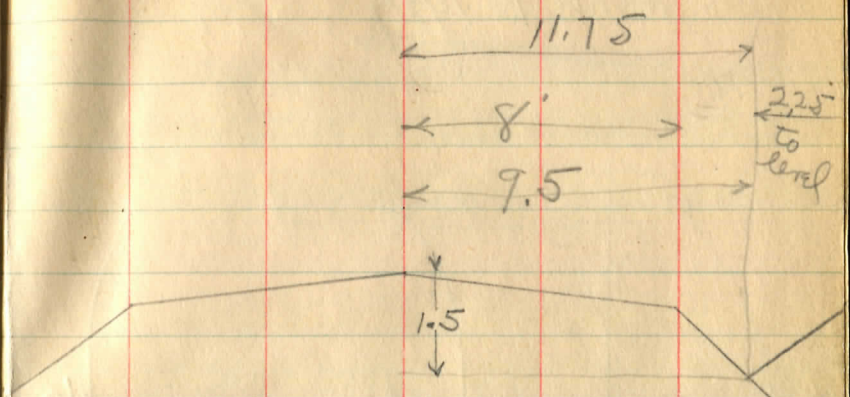
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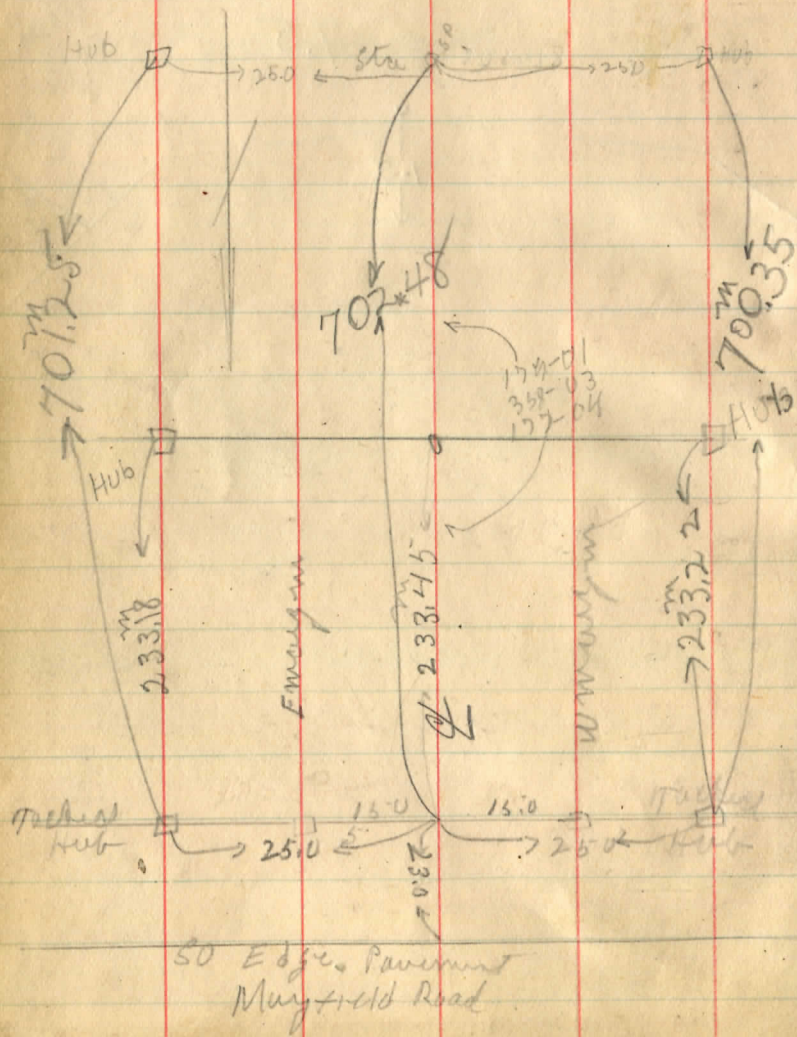
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Frank Butcher's Allotment Road

APRIL 1st 1927

Sta 16+41.42



Bliss
Goodrich
Clause

12" Tile culvert about Sta 1425
 Creek at 12+55 (culvert about 1226.)
 Bottom steep Bank 1265
 Top " " " "
 About 10 new hard maple ^{20"} Shingles
 But Stus 6+00 12+00
 Also 547 old rotten stumps

Reg'd 10 ft road bed
 together with ditches
 on 30 ft road.

537-04
 179-01-20

$16 + 26.5$
 25
 $16 + 51.5$
 3
 $13 + 51.5$

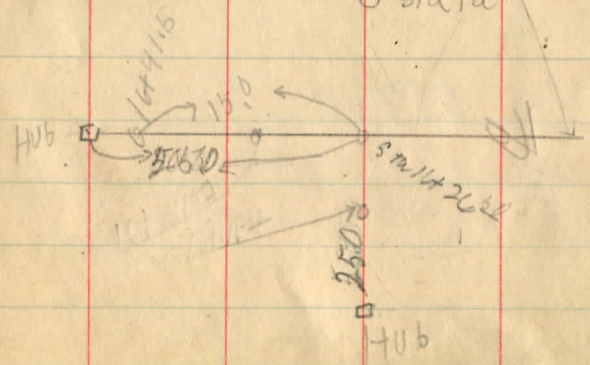
Cottrell's

Poor weather
 Cottrell's

104 + E + PL

92-22

o stata



Sta	BS	FS	HI	EI
BM	5.75		1222.63	1216.88
TP	1.90	2.15	1222.38	1220.48
TP	0.34	8.00	1214.72	1214.38
BIM 5.4	0.86		1213.86	1213.76
0-28	2.99		1211.70	1211.53
0-				
0-15	4.35		1210.37	
0-0	5.70	09.0		09.02
0+50	7.2		1207.52	
1+00	8.9		1205.82	
1+35	9.4		1205.32	
1+50	8.9		1205.82	
2+00	5.65		1209.07	
2+33.24	5.4		1209.32	
TP	0.36	4.91	1210.17	1209.71
3+00	1.80		1208.37	
3+50	2.60		1207.57	
4+00	3.30		1206.87	
4+50	4.13		1206.04	

attrails stone
 U.S. G.S. BM. NW corner Stone Foundation
 NE corner of step to church
 on Boulder
 NE corner Foundation mound well. Rem of stone
 Edge Pavement in pl.

	-15 E	-.05	0	+0.5 W	+0.1
	$\frac{4.53}{15.0}$	$\frac{4.54}{15.0}$	4.33	$\frac{4.30}{10}$	$\frac{4.23}{15}$
-20	$\frac{5.60}{15.0}$	$\frac{5.26}{10.0}$	5.20	$\frac{5.23}{10}$	$\frac{5.40}{15}$ +.30
+10	$\frac{7.10}{15.0}$	$\frac{7.10}{10}$	7.20	$\frac{7.30}{10}$ -10	$\frac{7.30}{10}$ -10
+20	$\frac{8.20}{15}$	$\frac{8.20}{15}$	8.20	$\frac{8.2}{10}$ -10	$\frac{8.00}{15}$ -10
+70	$\frac{8.70}{15}$	$\frac{8.40}{10}$	8.40	$\frac{8.60}{10}$ -20	$\frac{8.25}{15}$ -.35
+240	$\frac{7.50}{15}$	$\frac{7.20}{10}$	8.00	$\frac{8.60}{10}$ -70	$\frac{8.60}{15}$ -.70
+10	$\frac{5.50}{15}$	$\frac{5.20}{10}$	5.20	$\frac{6.00}{10}$ -35	$\frac{6.40}{15}$ -.75
+10	$\frac{5.30}{15}$	$\frac{5.30}{10}$	5.40	$\frac{5.20}{10}$ -25	$\frac{5.20}{15}$ -.35
00	1.20	00	1.20	$\frac{1.20}{10}$ 00	$\frac{1.20}{10}$ 00
-10	$\frac{2.70}{15}$	$\frac{2.60}{10}$	2.60	$\frac{2.30}{10}$ +.05	$\frac{2.30}{15}$ +.10
-10	$\frac{3.40}{15}$	00	3.30	$\frac{3.10}{10}$ +15	$\frac{3.10}{15}$ +20
+23	$\frac{3.40}{15}$	$\frac{3.40}{10}$	4.13	$\frac{4.30}{10}$ -17	$\frac{4.20}{15}$ -.27

139° FS HI EL

5700 510 1210¹⁷ 1205⁰⁷
 5+60 600 1209¹⁷
 6+00 700 1208¹³
 6+50 740 1202⁷⁷
 7+00 1025 1199⁹²

TP 0.20 942 1200²⁵ 1200²⁵

7+50 390 1197⁹⁵
 8+00 560 1193³⁵
 8+50 725 1193⁰⁰
 9+00 1170 1189²⁵

TP 0.23 1113 11900⁵ 1194⁷²

9+25 330 1186⁷⁵
 9+45 610 1183⁹⁵
 10+00 760 1182⁴⁵
 10+50 760 1182⁴⁵
 11+00 940 1180⁶⁵
 11+00 1100 1179⁰⁵

TP 3.15 970 1183⁵⁰ 1170³⁵

BM set 360 1174⁹⁰ B.M.

F E W
 +.05 $\frac{505}{15} = .05 \frac{515}{15}$ 310 $\frac{520}{10} = .10 \frac{510}{15}$ 00
 -.20 $\frac{620}{15} = .10 \frac{610}{10}$ 600 $\frac{540}{10} = +.10 \frac{545}{15} + .05$
 +.90 $\frac{610}{15} = +.105 \frac{595}{15}$ 700 $\frac{635}{10} = +.65 \frac{620}{15} + 1.00$
 -1.30 $\frac{770}{15} = -1.30 \frac{770}{15}$ 740 $\frac{760}{10} = .20 \frac{720}{15} + .20$
 +.25 $\frac{1000}{15} = .45 \frac{1020}{10}$ 1025 $\frac{1020}{10} = +.05 \frac{965}{10} + .60$
 +.40 $\frac{360}{15} = +.40 \frac{360}{10}$ 320 $\frac{340}{10} = +.40 \frac{360}{10} + 40$
 -.20 $\frac{570}{15} = -.10 \frac{570}{10}$ 560 $\frac{530}{10} = +.30 \frac{540}{15} + .20$

+ .60 $\frac{735}{15} = .00 \frac{745}{10}$ 525 $\frac{860}{10} = +.65 \frac{860}{15} + .65$
 +.50 $\frac{1120}{15} = +.40 \frac{1130}{10}$ 1120 $\frac{1240}{10} = .70 \frac{1240}{15} = .70$

+1.50 $\frac{190}{15} + .90 \frac{240}{10}$ 330 $\frac{520}{10} = .90 \frac{540}{15} = 1.70$
 +.230 $\frac{380}{10} + .180 \frac{430}{10}$ 610 $\frac{810}{10} = .200 \frac{810}{15} = .200$
 +.225 $\frac{530}{15} = +.165 \frac{595}{10}$ 760 $\frac{835}{10} = .75 \frac{860}{15} = .90$
 +.140 $\frac{620}{15} = +.100 \frac{640}{10}$ 760 $\frac{760}{10} = +.10 \frac{720}{15} = 1.60$
 00 $\frac{940}{10} = -.10 \frac{950}{10}$ 940 $\frac{1020}{10} = .80 \frac{1040}{15} = .70$
 -.20 $\frac{1120}{15} = -.30 \frac{1130}{10}$ 1100 $\frac{920}{10} = +.10 \frac{1010}{15} = .90$

+ on stone 330 W of line (15" E of 12" A.M.)

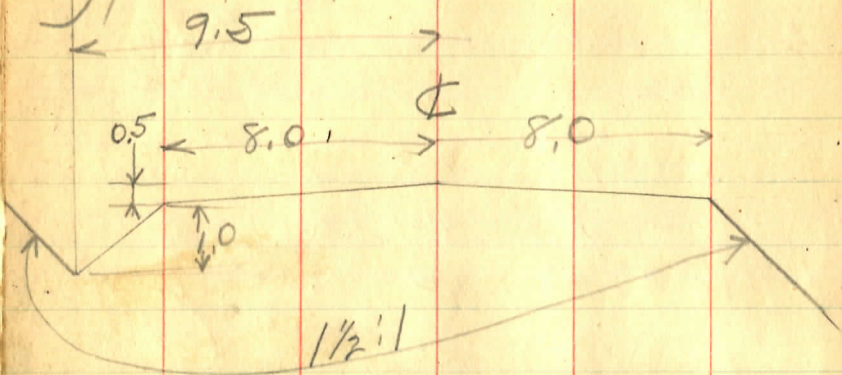
BS	FG	HJ	FL
11+60	<u>720</u>	1183 ⁵⁰	1176 ³⁰
12+00	<u>670</u>		1176 ⁸⁰
12+25	<u>790</u>		1175 ⁶⁰
12+50	<u>750</u>		1176 ⁰⁰
12+68	<u>810</u>		1175 ⁴⁰
12+68	<u>620</u>		1177 ⁷⁰
TP 00	1295	140	119505
13+00	<u>690</u>		1188 ¹⁵
13+50	<u>485</u>		1190 ²⁰
14+00	<u>375</u>		1191 ³⁰
TP	460	262	119203
14+50	<u>620</u>		1190 ⁸³
15+00	<u>670</u>		1190 ³³
15+50	<u>730</u>		1189 ⁷³
16+00	<u>700</u>		1190 ⁰³
16+41 ⁴⁰	<u>710</u>		1189 ⁹³
sta 1a	<u>570</u>		1191 ³³
2a	<u>340</u>		1193 ⁶³
BMS 4	<u>560</u>		1191.43

15'	F	Q	W	11
<u>40</u> > 60	<u>40</u> > 60	> 20	> 40 - 20	> 00 + 20
+20 > 60	+70 > 60	670	620 + 50	640 + 60
00 > 40 + 10	> 80	> 80	> 20 + 70	> 60 + 30
+130	630 - 95	> 80	> 60 + 40	> 20 + 30
		910	910	
+50	520 + 70	620	520 + 60	610 + 10
-100	> 40 - 80	> 20	640	620 + 70
+05	420 + 45	440	485	340 + 95
-105	470 - 65	410	322	330 + 45
-60	680 - 40	640	620	520 + 140
-50	> 20 00	620	620	530 + 95
-60	> 40 - 20	> 60	620	530 + 115
-80	> 70 00	> 00	620	620 + 30
00	> 10 + 20	640	710	620 + 50
			760 - 50	730 - 20
+10	540 + 10	540	570	510 + 60
+10	330 + 60	290	340	300 + 40

On Boulder 60' E of Fence 100 ft S of E of Road

Frank Battles Chester

Typical X Sec.



Sta	BS	HI	F.S.	Elev
BM	-	-		
			"	

13

B.S.	H.I.	F.S.	Elev
B.M.	-0.41	1213.45	1213.86
0+50W		5.67	1209.80
0+50E		5.18	"
1+00W		6.76	08.19
1+00E		6.76	"
1+50W		7.82	07.15
1+50E		5.30	07.15
2+00W	slope 14.75	4.76	06.69
2+00E	slope 15.5	3.27	06.69
3+00W		4.27	07.20
3+00E		4.75	07.20
4+00W		5.71	07.25
4+00E		6.22	"
5+00W		7.66	05.80
5+00E		7.68	05.80
6+00W		8.58	03.40
6+00E		9.05	03.40
T.P.	2.07	06.27	04.20
	1206.09		04.02

well
 N.E. corner found near of Bottles Store
 F 2.0 ✓
 F 1.5 ✓
 F 1.5 ✓
 F 1.5 ✓
 F 1.5 ✓
 C 1.0 ✓
 C 2.0 ✓
 C 3.5 ✓
 C 2.0 ✓
 C 1.5 ✓
 C 0.5 ✓
 G ✓
 G ✓
 G ✓
 C 1.5 ✓
 C 1.0 ✓
 on boulder 10ft E of sta 6+15

1206.09
~~1206.27~~

7+00W		6.22	1199.55	6.72
7+00E		5.76	99.55	"
8+00W		10.52	94.25	12.02
8+00E		10.51	94.25	"
T.P.	0.58	1196.70 1196.88	9.97	1196.12 1196.30
9+00W		7.63	88.75	8.13
9+00E		5.64	88.75	8.13
B.M.	0.60	1186.32 1186.50	10.98	1185.72 1185.90
10+00W		3.97	83.54	2.96
10+00E		1.95	83.54	"
11+00W		6.66	80.36	6.14
11+00E		6.15	80.36	"
12+00W		8.81	79.67	6.83
12+00E		10.84	79.67	"
B.M.		9.02	1177.30 1177.48	
T.P.	11.32	1194.05	3.59	1182.73
B.M.		2.61	1191.44	1191.43
B.M.	6.78	1184.08 1184.26	1177.30 1177.48	
B.M.		4.15	1179.93	1179.90

17

C 0.5
C 1.0
C 1.5
C 1.5
Top boulder 8+07+18 ft E of ϕ
C 0.5
C 2.5
SpK on S Root 36" Maple 9+80+44 E of ϕ
F 1.0
C 1.0
F 0.5
G
F 2.0
F 4.0
SpK in N.W. root 30" Map 11+75+40 ft E of ϕ
on Boulder 60 ft E. of Cottrell E fence and 45 ft S. of ϕ E+W TRS
SpK N.W. root 38" Map Sta 11+75 + on Boulder 11+15+35 ft W. of ϕ

These stakes set
0.18 ft. to low on check
of comp.

Battle PD
cont

✓
1195.87

13+00 E

9.99 83.88 C 2.0 ✓

13+00 W

5.96 1183.88 C 6.0 ✓

13+50 E

6.71 87.14 C 2.0 ✓

+50 W

3.74 87.14 C 5.0 ✓

14+00 E

5.53 89.84 C 0.5 ✓

14+00 W

3.50 89.84 C 2.5 ✓

15+00 E

5.72 91.15 F 1.0 ✓

15+00 W

4.70 91.15 G ✓

16+01 E

6.16 90.71 F 1.0 ✓

16+01 W

4.68 90.71 C 0.5 ✓

17+00 N

3.66 91.70 C 0.5 ✓

17+00 S

5.14 91.70 F 1.0 ✓

18+00 N

1.94 93.40 C 0.5 ✓

18+00 S

2.96 93.40 F 0.5 ✓

18+36.5 N

+36.5 S

✓ 1 ✓
4.42 91.45 1191.43

21

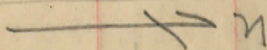
B.M.

BS
3.48

1180.78 1177.30

Topography Sewer

Street



1174.8
5.99
00

73.40

7.40
75

Creek

80 ft

74.30
+ 6.50
40

73.50

7.25
75

+ 4.95
80

75.63

7.13
100

76.00

9.00
150

73.8

7.00
95

74.95
5.05
100

70.73

1.05
175

71.60

9.20
200

73.83

6.95
200

PL

Creek

69.78

11.00
250

68.3

12.6
350

B.M.

3.48

BS F.S

Battles + Cottrell Allotment Preliminary Sewer Elev.

Weather:
Cold + Snow

Goodrich
clause
Rand

Sta	BS	HI	FS	Elev
B.M.	10.83	1188.13		1177.30
TP	11.19	1198.16	1.16	1186.97
TP	12.70	1209.05	1.81	1196.35
TP	8.05	1217.02	0.08	1268.97
0+00		"	2.46	1214.56
0+50		"	2.00	1215.02
1+00		"	2.37	1214.65
1+50		"	3.70	1213.32
2+00		"	5.20	1211.82
2+50		"	6.62	1210.40
3+00		"	9.05	1207.97
3+50		"	11.17	1205.85
TP	0.25	1207.12	10.15	1206.87
4+00		"	4.50	1202.62
4+50		"	6.67	1200.45
5+00		"	9.35	1197.77

Battles & Cottrell Survey 25
Remarks

{ Spk in NW Root 30" Map 11+75+
{ 40 ft E of ϕ (Road notes)

{ Cn ϕ of View Drive E Margins
{ of Chill. Road (Hub #1)

Sta	BS	HI	FS	Elev
5+50		1207.12	12.07	1195.05
TP	5.48	1201.87	10.73	1196.39
6+00		"	8.85	1193.02
6+43		"	9.40	1192.97
0+00		"	9.40	1192.97
0+16		"	10.65	1191.22
0+50		"	9.00	1192.87
1+00		"	6.65	1195.22
1+50		"	6.55	1195.32
2+00		"	5.27	1196.60
2+50		"	5.70	1196.17
3+00		"	5.85	1196.02
3+50		"	6.50	1195.37
3+91		"	6.75	1195.12 ✓
TP	12.43	1207.55	6.75	1195.12

Battles & Cottrell Sewer²⁷
Remarks

{ End of View Drive Hub on finer sections (Hub #2)

Going S from same point above on N. + S. Drive

← Hub #4

on Hub #2 Cottrell Drive + St. 90m N. on W Line of Battles

Sta	BS	HI	FS	Elev
TP	8.18	1215.58	0.15	1207.40

0+00	"		3.55	1212.03
------	---	--	------	---------

0+50	"		3.95	1211.63
------	---	--	------	---------

1+00	"		3.80	1211.78
------	---	--	------	---------

1+50	"		4.45	1211.13
------	---	--	------	---------

2+00	"		6.15	1209.43
------	---	--	------	---------

2+50	"		7.65	1207.93
------	---	--	------	---------

3+00	"		9.25	1206.33
------	---	--	------	---------

3+50	"		11.20	1204.38
------	---	--	-------	---------

TP	2.16	1204.99	12.75	1202.83
----	------	---------	-------	---------

4+00	"		3.65	1200.34
------	---	--	------	---------

4+50	"		5.95	1199.64
------	---	--	------	---------

5+00	"		5.80	1199.19
------	---	--	------	---------

5+50	"		6.95	1198.04
------	---	--	------	---------

6+00	"		8.95	1196.04
------	---	--	------	---------

TP	6+47.6	1.54	1196.66	9.86	1195.12 1195.13
----	--------	------	---------	------	--------------------

674-

Battles of Cottrell Sewers ²⁹
Remarks

On E of Cottrell Drive E Margin
of Ch. 171. road (Hub #3) going E

Hub #4

Sta	BS	HI	FS	Elev
0+00		1196.66	1.54	1195.12 ←
0+50		"	3.23	1193.43
1+00		"	4.10	1192.56
1+50		"	4.70	1191.96
2+00		"	5.36	1191.30
2+29.5		"	5.82	1190.84 ←
0+00		"	11.25	1185.41
0+50		"	9.00	1187.66
0+00		"	8.15	1188.51
1+50		"	8.05	1188.61
2+00		"	6.20	1190.46
2+10.1		"	5.82	1190.84
0+00		"	5.00	1191.66
0+50		"	5.20	1191.46
1+00		"	6.45	1190.21
1+50		"	6.50	1190.16
2+00		"	9.50	1187.16
2+50		"	13.80	1182.86

Battles & Cottrells Sewer 31

Remarks

Hub #4 going E on Cottrell Drive
Sta 6+47 on tan from chill. Rd.

Sta 8+76 " " " " "

Hub #5 Battles Drive &

Hub #6 on E end Cottrell Drive going W

Omit
not needed.

Hub #5

S end of Battles Drive going N (Marker)

Sta	BS	HI	FS	Elev
		1196.66		
3+00			11.50	1185.16
3+50			8.75	1187.91
4+00			6.40	1190.26
4+50			0.75	1189.91
4+59.8				1190.84
5+00			5.95	1190.71
5+50			5.85	1190.81
6+00			5.80	1190.86
6+50			6.30	1190.36
7+00			7.25	1189.41
7+50			10.00	1186.66
TI	1.09	1188.15	9.60	1187.06
7+75			3.00	1185.15
8+00			4.60	1183.55
8+25			6.15	1182.00
8+52			7.15	1181.00
8+70			7.90	1180.25
8+90			8.60	1179.55

Battles & Cottrell Sewers ³³
Remarks

Hub # 5

5' S ^(S side) of ⁶⁶ culvert on E of road
5' N ^(N side) " " " "

Sta	BS	HI	FS	Elev
		1188.15	9.25	1178.90
		"	12.90	1175.25
TP	3.57	1184.00	7.72	1180.43

0+00				1179.55
------	--	--	--	---------

0+10		"	6.05	1177.95
------	--	---	------	---------

0+20		"	7.10	1176.90
------	--	---	------	---------

0+55		"	8.70	1175.30
------	--	---	------	---------

0+75		"	8.80	1175.20
------	--	---	------	---------

0+95		"	8.45	1175.55
------	--	---	------	---------

1+27		"	8.00	1176.00
------	--	---	------	---------

1+52		"	8.20	1175.80
------	--	---	------	---------

1+72		"	7.60	1176.40
------	--	---	------	---------

0+00				1180.25
------	--	--	--	---------

0+10		"	9.95	1179.05
------	--	---	------	---------

0+20		"	9.20	1174.80
------	--	---	------	---------

0+36		"	9.25	1174.75
------	--	---	------	---------

0+56		"	8.30	1175.70
------	--	---	------	---------

0+91		"	9.50	1174.50
------	--	---	------	---------

Battles & Gattells Sewer ³⁵

Remarks

top of culvert E side

Flow line E side

Going E from Sta 8+90 along N side
of lot #36

N. Edge of creek

Fence line

Going E from Sta 8+70 (11 to Lot 36)

¢ of creek

¢ of creek

Sta	BS	HI	FS	Elev
-----	----	----	----	------

1+14		1184.00	8.70	1175.30
------	--	---------	------	---------

1+34			8.40	1175.60
------	--	--	------	---------

1+58			8.20	1175.80
------	--	--	------	---------

BM.			6.60	1177.30 ✓ 1177.40
-----	--	--	------	----------------------

0+00		1193.45	0.98	1192.47
------	--	---------	------	---------

0+25			3.10	1190.35
------	--	--	------	---------

0+50			3.40	1190.05
------	--	--	------	---------

0+75			4.00	1189.45
------	--	--	------	---------

1+00			2.90	1190.55
------	--	--	------	---------

1+25			3.10	1190.35
------	--	--	------	---------

1+50			3.40	1190.05
------	--	--	------	---------

1+75			3.40	1190.05
------	--	--	------	---------

2+00			5.00	1188.45
------	--	--	------	---------

2+10			6.00	1187.45
------	--	--	------	---------

2+14			9.30	1184.15
------	--	--	------	---------

2+19			11.30	1182.15
------	--	--	-------	---------

2+29			10.10	1183.35
------	--	--	-------	---------

Battles & Cottrells Sewer 37
Remarks

Spk N, W Rist 30" Maple Sta 11+75
40' E of (Road Notes)
Hub #2 gain E

top of bank.

Ditch

of Drive 58' S of Middle of culvert

Sta	BS	HI	FS	Elev
0+00				1192.47
0+50			3.2	
0+00			6.4	
1+32			6.0	
1+46			10.45	
1+61			16.50	
1+92			15.30	
0+00			0.98	1192.47
0+50			2.90	
0+75			6.30	
1+00			7.40	
1+21			8.60	
1+44			15.80	
1+59			17.1	

Battles & Cottrells Sewers ³⁹

Remarks

Hub #2 going E to 5' N of culvert

top of creek bank

of creek

point 20 W of Point 5' N of culvert
 (1st line on W Margin of road)

Hub #2 going E to Sta 8+90

top of bank

of creek

Battles Syfd.

F.S. HI

Topo for
Depth to
B.S. Elev.

6.74 1184.04

1177.30

a-1

9.04 75.00

b-1

6.83 77.21

c-1

7.95 76.09

d-1

7.83 76.21

e-1

7.28 76.26

f-1

8.21 75.83

g-1

9.91 (E. Creek 74.13)

h-1

9.21 (N. Edge H₂O 74.83)

i-1

8.65 (12 feet North of Creek 75.39)

j-1

7.21 76.83

a-2

9.98 74.06

b-2

8.74 75.30

c-2

8.24 75.80

d-2

8.40 75.64

e-2

9.28 74.76

f-2

8.79 (75.25) →

g-2

7.94 76.10

h-2

8.76 75.28

i-2

8.15 75.89

j-2

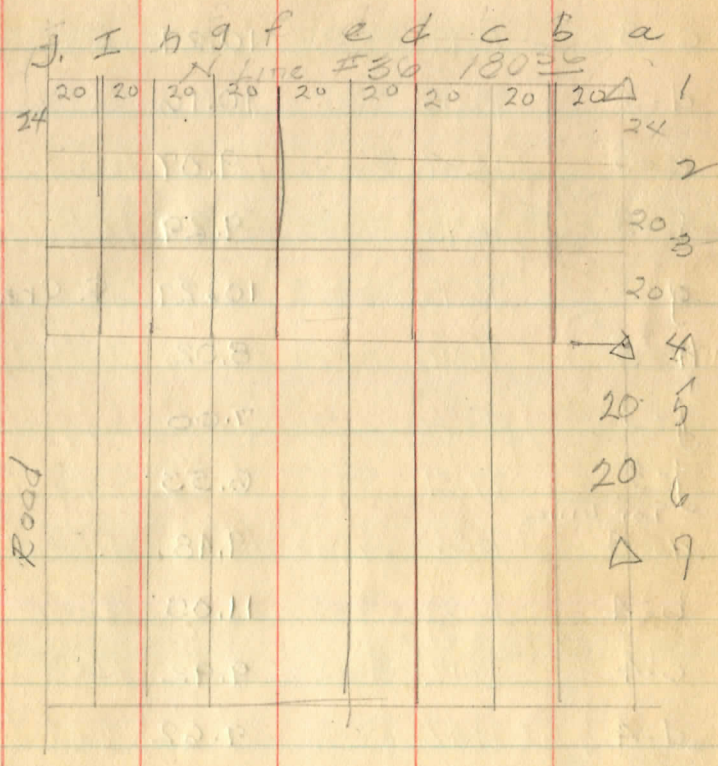
8.78 (3' N. E H₂O) 75.20

2-17-28

Root (road) (Stank level)

41

Spk N.W. root 30' Map 40 ft E. & + 48 ft N. of culv.



-(F-2 + 12' (West) 10.01 - E CREEK) (74.03)

(Continued)

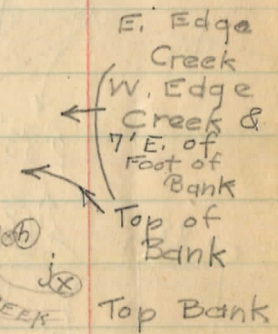
Topo - Battles Septic Tank

	<u>Elev.</u>	B.S.	<u>Elev</u>
a-3	74.21	9.83	
b-3	73.08	10.96	
c-3	73.75	10.29	
d-3	73.88	10.16	
e-3	74.97	9.07	
f-3	74.75	9.29	
g-3	73.75	10.29	£ Creek
h-3	76.02	8.02	
j-3	77.04	7.00	
j-3	77.51	6.53	
<u>Lot Line</u>			
d-4	74.56	9.48	
b-4	72.99	11.05	
c-4	74.12	9.92	
d-4	74.42	9.62	
e-4	74.60	9.24	
f-4	74.64	9.40	
g-4	74.39	9.65	E. Edge Creek
h-4	77.84	6.20	
i-4	77.55	6.49	
j-4	77.42	6.62	

(Continued)

43

	<u>Elev</u>	B.S.	
a-5	73.11	10.93	
b-5	72.92	11.12	
c-5	74.72	9.32	
d-5	74.03	10.01	
e-5	74.69	9.35	
f-5	73.96	10.08	
g-5	74.84	9.20	
h-5	81.72	2.323	
i-5	83.12	0.92	
j-5		-	
a-6	73.06	10.98	
b-6	72.72	11.32	
c-6	74.39	9.65	
d-6	74.40	9.64	
e-6	72.03	12.01	
f-6	74.13	9.91	
g-6	75.48	8.56	
h-6	81.85	2.19	
i-6	83.99	0.05	
j-6			



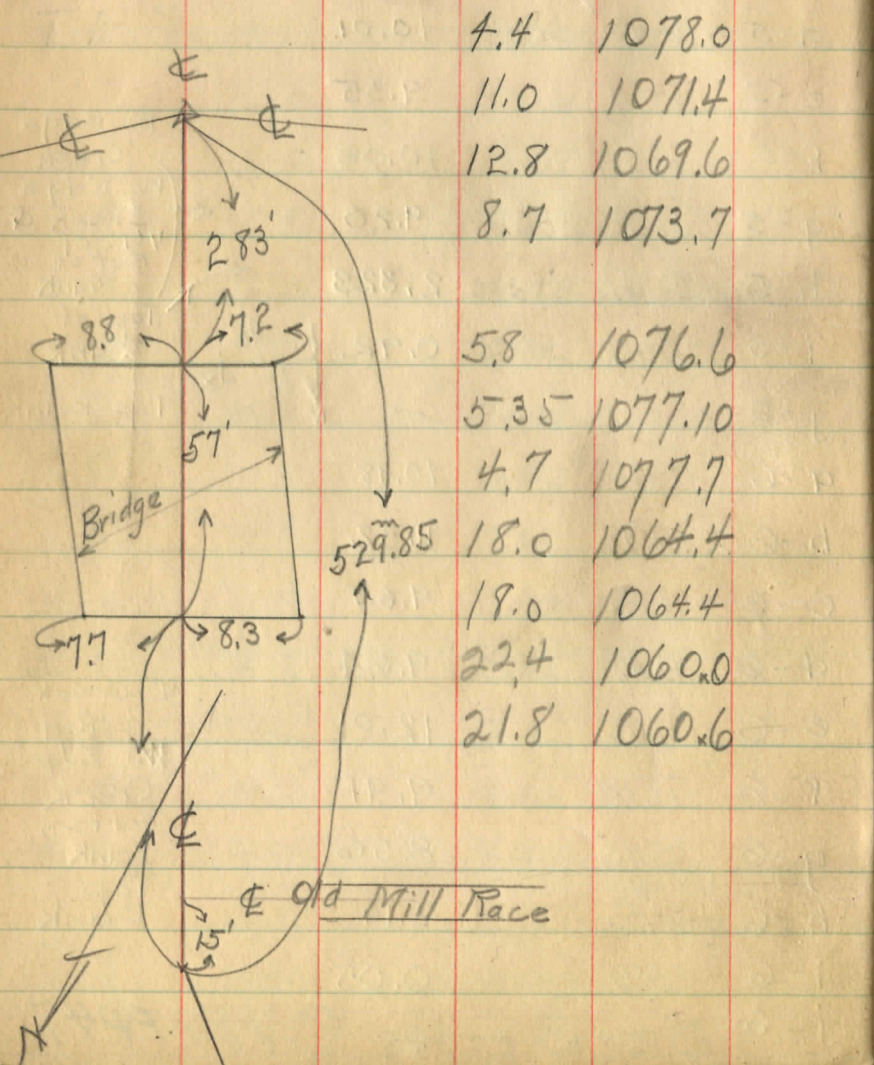
£ Creek Bed
 W. Edge Creek Bottom Bank
 Top Bank

See 3 pages OVER PP47

Levels at Fullertown Bridge

11/29/2745

Sta	BS	HI	FS	Elev
BM	2.93	1095.08		1092.15 ←
BM	0.43	1094.90	0.61	1094.47 (1094.44)
TP	0.53	1082.45	12.98	1081.92



4.4	1078.0
11.0	1071.4
12.8	1069.6
8.7	1073.7
5.8	1076.6
5.35	1077.10
4.7	1077.7
18.0	1064.4
19.0	1064.4
22.4	1060.0
21.8	1060.6

Spike on E root pine 50' N Store
 ← top of IP on 4 cor. SE Store,

- 15 ft N.W. on Rd & from & old Mill race
- 40 ft S.W. of Rd & in & Trace
- 80 " " " " " " " " " "
- On old dam Embkmt 150' N.W. of N. end bridge
- + 75' N.E. of Rd &
- 100 + 150 N.W. of N. end bridge on Rd &
- N. end bridge
- S. " "
- Surface Water W. side bridge
- " " E. " "
- Creek bed W. " "
- " " E. " "

1111

Elev

Continued from 347
Pages back

Lot Line	Elev	B.S.	
d-7	72.04	12.00	
b-7	72.40	11.64	
c	72.00	12.04	4 CREEK
d	77.63	6.41	Top Bank
e	79.35	4.69	
f	81.08	2.96	
g	82.84	1.20	
h		—	
i		—	
j		—	

Kent. (Nichols farm) Fullertown

1076819.19 67.6

0.57 76.24

3.82 73.0

8.82 68.0

T.P. 5.64 78.96 3.49 73.32

9.25 69.71

B.M. 5.07 73.89

B.M. 3.09 75.87

15.29 63.67

16.21 62.75

12.65 2.64
192

Danforth

Surf. H₂O Int. River + Creek at W. End

& Rd of Culvert at W. End Danforth

Top throat N. end Culvert 4 ft wide.

Bot. " " " "

High ground 150± E. of old Dam

Bent spk on stump on old Dam

S.E. & of N.W. Bridge abutmt. (Not parapet)

Surface H₂O at N.E. side bridge

Top grillage N.W. End bridge

Frank Battles Chesterland
Grade Stakes for Land

Sta.	B.S.	H.I.	F.S.	Elev	Mark
B.M	6 ²⁷	83 ⁵⁷ 3 <u>57</u>		77 ³⁰ 80 ⁰⁰ 79 ⁵⁰ ←	4
11+97					
11+48 1/2			429	79 ²⁵	3
11+00			295	80 ⁵⁹	4
10+25	10 ⁰⁴	93 ⁰⁰	057	83 ⁰⁰	5
9+50			710	85 ⁹⁰	5
9+00			456	88 ⁵⁰	5
8+50			096	92 ¹⁰	6
T.P	129 ²	104 ⁹³	105	92 ⁰¹	6
8+00			923	95 ⁷	7
7+50			663	98 ³⁰	7
7+00			403	100 ⁹	7
6+50			173	103 ²⁰	8
6+00			043	104 ⁵	8
T.P	77 ⁶	111 ⁷⁴	095	103 ⁹³	
5+50			594	105 ⁸⁰	8
5+00			464	107 ¹⁰	8
4+50			534	106 ²	9

Can. 2 pgs over

5/22/28 + 5/23
on Battles "Opp- Locks Alley" Stks 5' W of #

11+7540'E
Spk NW root 30" Maple Stump 150' NE Culvert
See Next Page full
M.H.# 7 (2 stks to same grade 3' apart)

M.H

- 83.5
- 86.1
- 88.7
- 91.3
- M.H 93.9
- 95.2
- 96.5
- 97.8
- 99.1
- M.H. 00.4

Frank Battles Chesterland

Grade
Flow line

57

Sta	BS	HI	F.S	Elev	Mark
A+00		1211.74	4.14	1207.6	▽
B+50			2.94	1208.2	▽
3+00			2.74	1209.0	▽
2+50			3.54	1208.2	▽
BM			1.42	1210.32	←
2+00			3.34	1205.4	▽
1+50			3.14	1205.6	▽
1+00			2.94	1208.2	▽

00.6
00.8
01.0
01.2
01.4
01.6
01.8

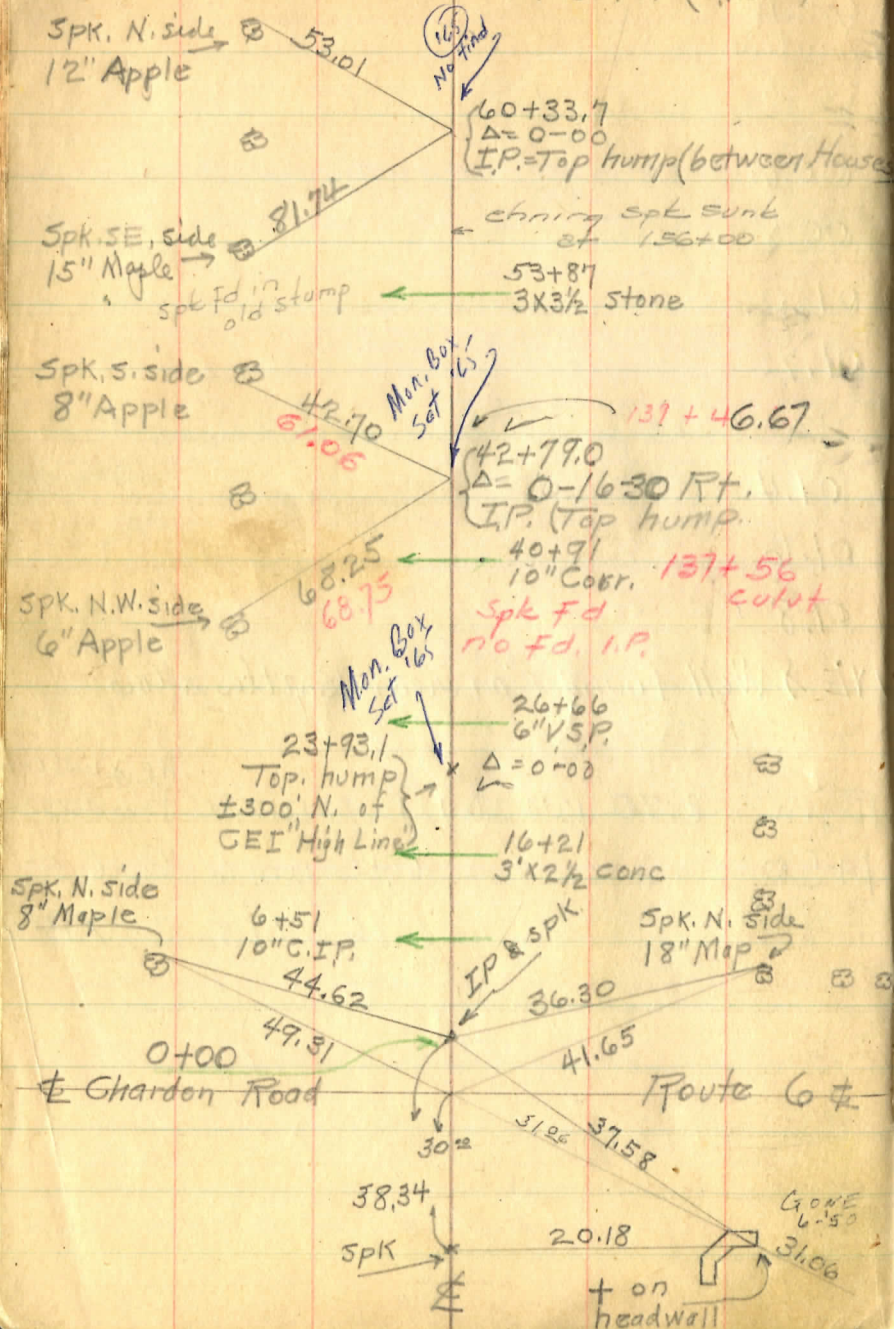
Top NW cor Stone pillar under NW cor porch house Lot 8.

-0.64 7/2/28 FR3 + 2 Pm.
1213.82 1213.86

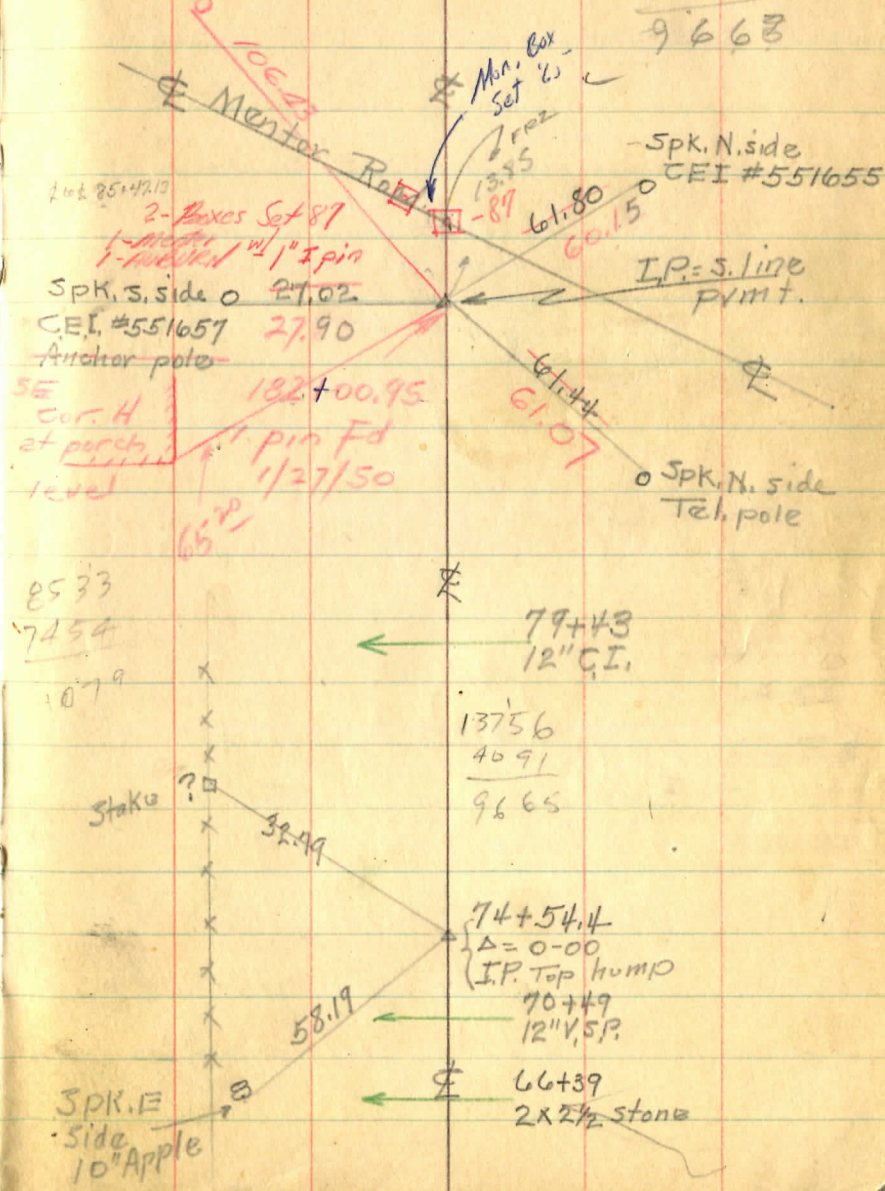
NE & Well foundation rear Battles store

		1213.82	3.46	1210.36	← 1210.32
4+00			4.85 +8.00	1200.97	4" high
3+50			5.02	00.8	C=8.0
3+00			4.82	01.0	C=8.0
2+50			5.60	01.2	C=7.0
2+00			5.42	01.4	C=7.00
1+50			6.22	01.6	C=6.00
1+00			5.02	01.8	C=7.0

B.M.	0.70	1214.56	1213.86	1213.86	NE & well foundation
1+50			6.46	1201.6	C=6.5
			5.76	01.8	C=7.0



Spk W side CEI -



Russell Farms Bench Marks
5/28/28 G.L. Bloor & H. Clouse

63

Sta	B S	HI	FS	EL
BM	12.97	1095.13		1082.16
TP	3.76	1091.10	7.78	1087.36
#7 BM	0.16	1084.36	6.41	1084.19
TP	0.47	1072.07 ³³	12.49	1071.86
TP	1.48	1061.44 ⁷⁶	12.16	1059.96
#6 BM	2.37	1057.00 ^{1057.00}	7.13	1054.31 ⁶³
TP	12.41	1068.44 ⁷⁶	0.66	1056.03 ³⁵
TP	11.82	1078.82 ^{79.24}	1.34	1067.46 ⁴²
TP	11.18	1088.90 ^{89.22}	1.20	1077.72 ^{78.14}
#8 BM	12.85	1101.44 ³¹	0.76	1088.14 ⁴⁶
TP	11.38	1112.40 ²²	0.47	1101.02 ^{1101.84}
TP	5.50	1117.10 ^{16.92}	0.80	1111.60 ⁴²
#4 BM	11.78	1126.42 ²⁴	2.46	1114.64 ⁴⁶
TP	11.86	1136.59 ⁴¹	1.69	1124.73 ⁵⁵
TP	11.92	1147.87 ⁶⁸	0.64	1135.73 ⁷⁷
#3 BM	8.54	1156.37 ¹⁶	0.07	1147.80 ⁶²
TP	10.12	1163.02 ^{62.84}	3.44	1152.90 ⁷²
TP	11.57	1173.68 ⁵⁰	0.91	1162.11 ^{61.93}

T on SW Cor. N. Headwall. 3rd Tier From Top
Culvert at Foot Manchester Hill
on Boulder 75 ft W of Line. 10 ft 50 of wire ^{Frame}

Two spikes in NW Root 36" Maple 50' N of Creek

2 spikes in E Root 30" Elm. W of Ravine. (W. part split off)

2 spikes in E Root 30" Maple 75' W of Line at KA 50 of Ravine

2 spikes in W Root 24" Cherry 50' E of HA

	BB	HI	FS	EL
TP	0.99	1167.85 ⁵⁷	6.22	1166.46 ⁵⁸
#2 BM	9.27	1176.91 ⁵⁸	0.46	1167.31 ⁵⁹
TP	0.12	1172.65 ⁴⁷	4.23	1172.53 ⁵⁵
TP	11.41	1172.85 ⁶⁷	6.21	1166.44 ⁶⁴
TP	5.83	1191.68 ⁵⁰	2.00	1176.86 ⁶⁷
#1 BM			5.98	1175.70 ⁵²

Return

#1 BM	5.98	1191.68		1175.70 ⁵²
TP	0.80	1178.68	3.90	1177.37 ⁷⁰
TP	10.41	1178.74	11.35	1167.37 ¹⁵
TP	1.20	1174.44	4.50	1173.24
BM#2			6.44	1167.50 ³²
TP	2.71	1167.53	9.62	1164.82
TP	4.19	1171.32	0.40	1167.13
TP	1.33	1161.00	11.65	1159.67
TP	0.06	1148.71	12.35	1148.65
#3 BM			0.93	1147.78 ⁶⁰
TP	0.31	1137.77	11.25	1137.46

Take 0.18' from these readings.

#2 BM
2 SPINES in E Root 20' Maple 50 W of DA

BM#1 Ton Rock 75' N of NW corner Barn

BS HT FS EL

TP 0.15 1125.57 12.36 1125.42

TP 1.50 1117.95 9.32 1116.23

#4 BM 4.27 1113.⁴⁹~~67~~ 1114.46

TP 1.76 1111.07 8.64 1109.31

TP 0.41 1100.22 11.26 1099.81

#6 BM 0.55 1098.27 12.60 1097.⁵⁴~~77~~ 1099.46

TP 0.36 1059.15 9.99 1058.29

TP 0.45 1068.62 11.00 1068.15

TP 0.08 1056.46 12.24 1056.38

#6 BM 2.61 1053.⁶⁷~~78~~ 1044.31

TP 10.86 1066.27 1.04 1055.42

TP 12.75 1078.74 0.29 1065.49

TP 13.03 1091.32 0.45 1078.29

#7 BM 7.88 1083.²⁶~~44~~ 1084.14

TP 6.30 1092.93 4.69 1086.63

BM 12.49 1080.²⁶~~44~~ 1082.16

68

69

LEVELS ON CREEK - RUSSELL FARMS

Ellis
Foot
Stark K

6/11/28

	B.S.	H.I.	F.S.	ELEV.
BM. # 6	5.64	1061.30		1055.66
T.P.	9.91	1066.26	4.35	1056.95
T.P.	3.84	1063.18	7.52	1059.34
			5.28	1057.90
			6.53	1056.65
			2.47	1060.71
				4.06

WATER
SURFACE
AT
PROP. LINE
CREEK
BED AT
PROP. LINE
TOP BANK
SOUTH
Side Creek

ROAD - RUSSELL FARMS (Russell Twp)

STATION	B.S.	H.I.	F.S.	Elev.	B.M. #
B.M. #1	12.28	1189.84		1177.56	#1

T.P. 2.54 1185.32 7.06 1182.78

T.P. 0.53 1172.79 13.06 1172.26

T.P. 2.21 1162.65 12.35 1160.44

STATION	Left (West)		Right (East)	
0+00	3.5 <u>30</u>	2.8	1.8 <u>30</u>	± of E.W. Road
0+14	2.5 <u>30</u>	2.0	1.0 <u>30</u>	TOP DITCH BANK
1+00	4.2 <u>30</u>	3.9	4.5 <u>30</u>	
2+00	8.0 <u>30</u>	8.8	8.2 <u>30</u>	
2+40	10.8 <u>30</u>	11.0	9.5 <u>30</u>	
3+00	10.2 <u>30</u>	9.3	8.8 <u>15</u>	
4+00	8.9 <u>30</u>	8.0	7.8 <u>12</u>	
5+00	6.8 <u>30</u>	6.7	6.7 <u>15</u>	
5+35	9.2 <u>30</u>	8.7	7.8 <u>15</u>	
6+00	1.5 <u>30</u>	6.7	6.2 <u>15</u>	
6+60	7.0 <u>30</u>	4.7	4.3 <u>15</u>	
7+00	9.0 <u>30</u>	6.8	6.3 <u>15</u>	
7+60	3.2 <u>30</u>	2.2	1.8 <u>15</u>	
7+85	10.2 <u>30</u>	8.0	8.1 <u>15</u>	
8+00	3.2 <u>30</u>	3.2	3.1 <u>15</u>	

TOP SOUTH BANK OF RAVINE

TOP KNOLL

ROAD - RUSSELL FARMS

STA. B.S. H.I. F.S. ELEV.

T.P. 0.39 1152.62 10.42 1152.23

T.P. 2.11 1143.99 10.74 1141.88

T.P. 9.53 1151.76 1.76 1142.23

T.P. 11.12 1162.55 0.33
3.03 1151.43

T.P. 11.07 1172.86 0.76 1161.79

Note - Error in this F.S. of 2.70 feet
Correct figure is F.S. 0.33
DR Stark

T.P. "A" 15.73 1179.09 9.50 1163.36

T.P. "A" (Above) 7.96 1171.32

Note: - No new F.S. Used
B.S. or taken on last T.P. as shown 7.96
B.S. on this elevation

← Add 7.96 to

this elev for this

Note
at 58 and 8+90
taken with this
H.I. - 1143.99

West \oplus East \ominus

STA.

8+25

8+58

8+90

9+00

9+15

9+70

10+00

10+60

11+00

12+00

12+40

13+00

13+40

14+00

13+40

14+00

15+00

	+18	+19	-16	-31
	9.5	9.4	12.9	14.4
	30	15	15	30
	-20	-08	+08	+14
	7.1	6.3	4.3	2.7
	30	15	15	30
	-12	-14	+09	+16
	6.5	6.4	3.7	3.1
	30	15	30	40
	12.3	11.7	10.1	10.8
	40	30	15	40
	-08	-31	-13	-22
	5.1	4.5	9.9	10.8
	30	15	15	30
	-14	-05	+07	+14
	4.7	3.8	2.6	1.9
	30	15	15	30
	-47	-28	+08	+23
	4.5	11.3	4.0	8.5
	30	15	30	40
	13.6	11.3	11.2	6.9
	40	30	15	50
	-46	-31	+12	+37
	13.8	11.5	5.8	3.3
	30	15	30	40
	-48	-43	+12	+27
	4.0	11.2	7.5	5.1
	30	15	15	40
	13.4	12.7	11.2	1.3
	40	30	15	40
	-55	-44	+21	+53
	14.0	11.7	5.9	3.3
	30	15	30	40
	-31	-30	+18	+18
	13.1	13.0	8.2	4.3
	30	15	15	40
	40	30	15	10.0
	13.5	10.2	8.7	10.5
	40	30	40	50
	13.5	10.2	8.7	6.4
	40	30	40	50
	6.2	4.5	2.3	1.3
	15	30	40	50
	-6.0	-3.7	9.0	7.3
	13.3	11.0	9.0	7.3
	45	30	12	3.0
	-10.4	-8.1	7.3	3.8
	11.2	8.4	11.3	3.0
	50	40	30	15
	4.4	3.4	1.9	
	50	40	30	

See 13+40 & 14+00 below

Repeat Station

Bottom of Ravine South Side

ROAD - Russell Farms

STA.	B.S.	H.I.	F.S.	ELEV.
T.P.	10.49	1180.47	1.34	1169.98
B.M. (Set)			5.96	1174.51
T.P.	4.79	1181.68	3.58	1176.89
T.P.	5.92	1181.11	6.49	1175.19
T.P.	6.48	1181.18	6.41	1174.70
T.P.	6.97	1181.34	6.81	1174.37
B.M.#2			12.04	1169.30

MAY 31st 1928

ELISS C.F.
STARK
CLAUSE { Cool
Clear
Windy

B.M.#2	6.80	1176.16		1169.36
T.P.	2.62	1167.75	11.03	1165.13

STATION	West	+	(East)	
15+00	$\frac{56}{50} + \frac{56}{40} + \frac{41}{30} = \frac{153}{15}$	-19	+1	+46
B.M.	Spike	N.F. Post	10" Hard Maple	Stump (Sta. 15+10)
15+50	$\frac{62}{50} - \frac{33}{40} - \frac{26}{30} = \frac{51}{15}$	+21	0.6 + 45	+70
16+00	$\frac{52}{50} - \frac{27}{40} - \frac{18}{30} = \frac{51}{15}$	+20	3.4 + 46	+56
17+00	$\frac{67}{50} - \frac{38}{40} - \frac{21}{30} = \frac{51}{15}$	+15	2.1 + 46	+51
17+50	$\frac{87}{50} - \frac{13}{40} - \frac{55}{30} = \frac{51}{15}$	+22	3.4 + 39	+51
18+00	$\frac{74}{50} - \frac{60}{40} - \frac{32}{30} = \frac{51}{15}$	+16	3.3 + 39	+45
19+00	$\frac{89}{50} - \frac{40}{40} - \frac{33}{30} = \frac{51}{15}$	+30	4.3 + 51	+61
B.M.#2	30' West	Sta. 18+80	El. = 1169.36	

B.M.#2 (See Above)	+28	+67	+85	+105
19+50	$\frac{78}{50} - \frac{55}{40} - \frac{53}{30} = \frac{35}{15}$	9.2	5.3	3.5
OK		11.4	3.0	1.8

Repeat Sta.	$\frac{103}{50} - \frac{155}{40} - \frac{72}{30} = \frac{153}{15}$			
19+50	$\frac{114}{50} - \frac{101}{40} - \frac{89}{30} = \frac{153}{15}$			
20+00	$\frac{49}{50} - \frac{37}{40} - \frac{16}{30} = \frac{153}{15}$	+21	+39	+50
20+50	$\frac{41}{50} - \frac{23}{40} - \frac{19}{30} = \frac{153}{15}$	+15	+29	+42

ROAD - Russell Farms

STA.	B.S.	H.I.	F.S.	ELEV.
T.P.	7.20	1170.05	4.90	1162.85
T.P.	8.20	1174.91	3.34	1166.71
T.P.	6.65	1176.58	4.98	1169.93
T.P.	2.98	1173.84	5.72	1170.86
T.P.	7.06	1170.79	10.11	1163.73
T.P.	5.49	1166.42	9.86	1160.93
T.P.	3.10	1162.06	7.46	1158.96
Bottom Ravine				
T.P.	2.50	1156.66	7.90	1154.16

(West) \pm (East)

STATION	West		East		West		East		
21+00	-4 ¹ 10.7 40	-3 ¹ 9.7 30	-2 ¹ 8.7 15	+2 ⁸ 1163.5 6.6	+1 ⁸ 3.8 15	+1 ⁸ 1.8 30	-0 ⁴ 7.0 40		
22+00	-6 ³ 13.7 50	-5 ⁶ 13.0 40	-3 ⁹ 11.3 30	-2 ¹ 9.5 15	+2 ⁵ 1167.5 7.4	+1 ² 4.9 15	+5 ⁰ 2.4 30	+5 ⁶ 1.8 40	+6 ² 0.5 50
23+00	-5 ⁵ 10.8 40	-3 ⁸ 9.4 30	-2 ¹ 7.7 15	+1 ² 1171.0 5.6	+3 ⁴ 3.7 15	+3 ⁴ 2.2 30	+3 ⁹ 1.7 40		
(Note: - Sta. 23+65 \pm depression 10' wide and 1/2 foot deep (old wagon road))									
24+00	-5 ⁰ 11.3 50	-4 ¹ 10.1 40	-2 ² 7.2 30	-1 ⁴ 5.7 15	+1 ⁵ 1169.5 4.8	+2 ⁸ 2.8 15	+2 ⁸ 1.5 30	+0 ⁶ 0.6 40	+3 ¹ 0.6 40
25+00	-5 ⁶ 13.2 40	-4 ⁰ 11.6 30	-2 ¹ 9.7 15	+1 ¹ 1163.2 7.6	+3 ⁸ 5.9 15	+4 ⁶ 3.8 30	+4 ⁶ 3.0 40	+6 ⁰ 1.6 50	
26+00	-A ⁶ 11.9 40	-3 ¹ 10.4 30	-1 ³ 8.6 15	+2 ¹ 1159.1 7.3	+3 ⁵ 5.2 15	+4 ⁴ 3.8 30	+4 ⁴ 2.9 40		
(Note - Sta 26+00 - 26+50 Outcrop of bedrock (Sandstone))									
26+50	-5 ⁵ 13.2 50	-4 ¹ 11.6 40	-3 ³ 9.7 30	-1 ³ 8.7 15	+0 ⁸ 1157.3 4.8	+1 ⁸ 1.8 30	+2 ¹ 2.1 40	+2 ¹ 2.1 50	
26+80	-A ¹ 13.2 50	-A ⁶ 11.6 40	-3 ¹ 9.7 30	-1 ³ 8.7 15	+2 ¹ 1151.3 10.8	+6 ⁴ 6.4 30	+6 ⁵ 6.5 40	+6 ⁸ 6.8 50	
27+00	-5 ⁸ 14.7 50	-4 ³ 12.5 40	-2 ⁰ 10.2 30	+1 ⁰ 1153.9 8.2	+6 ³ 6.3 15	+2 ⁵ 5.6 30	+2 ⁵ 5.2 40	+2 ⁸ 5.4 50	
27+15	-5 ⁵ 8.5 40	-3 ⁶ 6.6 30	-1 ⁴ 4.1 15	+0 ⁹ 1153.7 3.0	+0 ⁹ 2.1 15	+1 ⁴ 2.1 30	+1 ⁴ 1.6 40	+1 ¹ 1.9 50	

ROAD - RUSSELL FARMS

STA. B.S. H.I. F.S. ELEV.

T.P. 3.53 1152.49 7.70 1148.96

RAVINE

T.P. 5.24 1150.00 7.73 1144.76

B.M.#3 0.39 1149.61

Sea F.S. on B.M.#3 above

B.M.#3 0.39 1150.03 1149.64

T.P. 3.80 1146.42 7.41 1142.62

T.P. 1.35 1135.83 11.94 1134.48

Small Gully West of E

T.P. 1.45 1127.41 9.87 1125.96

STATION	W	+	E	+	+
P.C.	-29	-16	-01	+09	+19
27+26	8.3	1.0	5.5	1151.3	4.5
27+50	-11	-11	-11	-05	+24
27+62	10.1	10.8	10.5	10.5	1147.6
28+00	-102	-62	-45	-16	+21
28+20	18.2	14.7	12.3	9.4	1144.7
28+35	-73	-53	-20	+18	+43
BM#3 - V	-41	-39	+15	+05	+46
29+00	11.0	10.5	10.5	10.5	1142.0
	11.0	10.5	10.5	10.5	1147.6
	50	40	30	15	4.9
					15
					30
					40
					50
					1.6
					6.2
					4.5
					3.2
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					6.2

ROAD - Russell Farms

STA. B.S. H.I. F.S. ELEV.

B.M.#4 11.94 1115.47
BLISS G.P. [Cool-Cloudy-Rain]
STARK
CLAUDE - NORTHERLY

T.P. 1.16 1111.86 7.03 1110.70

Temporary B.M.#4A 10.21 1101.65

STATION	West	East	CLASH
34+00	7.0 30	6.1 15	1121.8 4.6 3.8 30
34+00	-14/30	-05/15	+19/15 +18/30
35+00	8.71 30	7.9 15	1120.5 5.5 14 5.819
36+00	-1/30	-02/15	10.2 10.2 1117.7 9.5 +02 9.4 +03 30

B.M.EI. = 1115.48
B.M.#4 75' W. Sta. 36+50 E. Root 24' Maple

FROM STA. 36+52.50

E.M. EL. = 1115.48

B.M.#4	See Above	50'	+0.1	-0.5	+0.1
37+00	11.1 50	4.05 30	4.1 15	1113.2 4.6 4.4 5.0 4.4	5.0 4.4
37+50	5.4 50	6.5 40	6.2 30	111.6 6.1 6.1 6.1	-0.2 -0.3 -0.5 -0.2
38+00	2.3 40	2.3 30	2.3 15	1108.8 2.0 2.5 2.7	+0.3 +0.3 +0.3 +0.3
38+20	4.1 50	4.1 40	4.1 30	1107.1 2.9 2.7 2.8	-2.7 -2.7 -2.7 -2.7
38+40	4.1 50	4.1 40	4.1 30	1106.1 5.2 5.8 5.8	-1.4 -1.4 -1.4 -1.4
38+50	5.0 50	4.7 40	4.7 30	1101.3 10.6 10.6 10.6	+2.6 +2.6 +2.6 +2.6
38+60	5.2 50	5.2 40	5.2 30	1094.9 11.3 11.3 11.3	+3.2 +3.2 +3.2 +3.2
38+70	6.5 50	6.5 40	6.5 30	1088.5 17.0 17.0 17.0	+4.1 +4.1 +4.1 +4.1
38+90	9.0 50	10.2 50			

SILVERCREEK ROAD - (Russell Farms)

STA.	B.S.	H.I.	F.S.	ELEV.
TEMP. BENCH "4-A" See pg. 82 for elevation	3.69	1105.34		1101.65

T.P. 0.73 1094.64 11.43 1093.91

T.P. "Z" 2.12 1092.52

BLISS
ROOT
STARKA JUNE 7th 1928 -

T.P. "Z" 8.78 1101.30 1092.52

JUNE 8, '28

T.P. "Z" 6.69 1099.21 1092.52

West East

STATION

	-7.0	-5.4	-3.3	-2.3	-1.5	+0.6	+1.8	+1.8	+2.7	
	10.6	9.0	6.7	5.4	5.1	1101.7	3.0	1.8	0.9	✓
40+05	60	50	40	30	15	3.6	1.5	3.0	4.0	5.0
		-2.2	-1.6	0	-0.6	+0.5	+0.7	+0.6	+0.4	+0.1
		7.7	7.1	6.1	-1.2	1099.8	5.0	4.6	5.1	5.6
40+50		50	40	30	15	5.5	1.5	3.0	4.0	5.0
	-1.0	-0.8	-0.5	0	0	1095.0	-0.2	-0.6	-0.3	-0.2
	11.3	7.1	10.8	10.3	10.9	1095.0	0.5	-0.6	10.6	10.5
41+00	60	50	40	28	12	10.3	1.5	3.0	4.0	5.5

	-10.4	-7.1	-2.4	-1.3	-1.0	+0.9	+1.9	+2.2	+2.7	
	15.2	11.9	7.2	6.1	5.8	1089.8	3.9	2.7	2.6	2.1
41+50	65	50	43	30	15	4.8	1.5	3.0	4.0	5.0
		-14.4	-9.3	-5.3	-2.0	+1.4	+2.5	+3.1	+3.8	
		21.4	16.9	12.7	7.1	1089.0	4.2	3.5	2.5	3.8
41+65		50	40	30	17	5.6	1.5	3.0	4.0	5.0
	-11.9	-5.8	-2.5	-0.8		1090.4	+1.2	+1.6	+2.2	+3.1
	16.1	10.0	6.7	5.0		1090.4	2.0	2.6	2.0	1.1
41+80	46	35	28	15	4.2		7	2.0	3.0	4.0
										5.0

T.P. On Hardhead 6 feet E. Sta. 42+00

	1091.1	+1.3	+2.0	+2.8	+2.9					
	8.9	8.2	7.4	7.3						✓
42+00	10.2	15	30	40	50					
	1089.4	+2.3	+3.9	+4.7	+5.2	+5.8				✓
42+15	11.9	5	15	30	40	50				
	1087.7	+4.8	+6.9	+8.5	+8.9					✓
42+30	13.6	7.8	2.0	4.0	5.0					

	1086.5	+2.7	+8.5	+10.7	+11.3	+12.0				
	10.6	4.2	2.0	1.4	0.7					✓
42+50	12.7	5	2.5	4.0	5.0	6.0				

SILVERCREEK ROAD - (Russell Farms)

STA. B.S. H.I. F.S. ELEV.

T.P. "Z" 0.31 1092.83 1092.52

T.P. 2.48 1090.47 4.84 1087.99

T.P. 2.35 1080.30 12.52 1077.95

West & East

STATION

	1087.3	+6.5	+6.9	+7.4	
		5.4	5.0	4.5	
42+65	11.9	2.5	4.0	5.0	
	1088.6	+1.1	+1.0	+1.4	+2.3 +2.2
		9.5	9.6	9.2	8.3 8.4
42+85	10.6	10	20	30	40 50

	-25.2	-15.5	-13.5	
	27.0	17.3	15.3	1091.0
42+00	5.5	4.0	3.0	1.8
	-22.5	-20.0	-16.4	
	22.0	23.5	19.9	1089.3
+15.	5.5	4.7	3.0	3.5
	-20.0		27.0	1087.7
+30	25.1		30	5.1
	-18.9	-17.1		
	23.4			1086.5
-50	5.0	3.0	6.3	
	-18.0	-17.7	-16.1	
	23.5	23.2	21.6	1087.3
+65	5.0	4.0	3.0	5.5
	-13.2	-10.9	-10.5	
	1.5	15.2	14.8	1088.5
+85	5.5	4.5	3.3	4.3

	-9.5	-4.1	-2.0	+0.3	
	12.6	7.2	5.1	2.8	1087.4
43+00	6.0	4.0	3.0	1.8	3.1
	-9.2	-6.0	-3.4	-0.9	+0.5
	12.7	1.5	6.7	5.4	3.0
43+10	5.0	4.0	3.0	3.5	1.5
	-1.4	+0.7	+0.7	+0.1	+0.2
	8.1	6.6	1.1	1.1	1.1
43+25	5.0	4.0	3.0	1.5	1.3
	+1.0	+0.8	+0.8	0	0
	10.9	16.1	11.1	11.9	10.3
43+45	5.0	4.0	2.7	1.5	11.9
	+5.7	+5.4	+3.5	+1.4	1073.6
	1.0	1.3	3.2	5.3	7.9
43+55	5.0	4.0	2.0	1.0	6.7
	+8.7	+8.5	+6.7	+1.3	1067.5
	4.1	4.3	6.1	11.5	12.0
43+68	5.0	4.0	3.0	1.5	12.8
	+8.2	+7.2	+1.9	-0.7	1065.3
	6.8	7.8	13.7	15.7	16.5
43+85	6.5	5.3	3.0	1.5	15.0

	-1.1	-2.8	-4.1	
	7.8	9.5	10.8	Edge of
43+55	5.0	4.0	2.0	1.0
	+8.7	+8.5	+6.7	+1.3
	4.1	4.3	6.1	11.5
43+68	5.0	4.0	3.0	1.5
	+8.2	+7.2	+1.9	-0.7
	6.8	7.8	13.7	15.7
43+85	6.5	5.3	3.0	1.5

SILVERCREEK ROAD - (Russell Farms)

STA. B.S. H.I. F.S. ELEV.

1.86 1069.81 12.35 1067.95

T.P. 0.47 1059.70 10.58 1059.23

T.P. 4.22 1058.96 4.96 1054.74

B.M.#6 3.34 1055.62

B.M.#6 3.34 1059.00 1055.66

NOTE

T.P. 10.23 1066.26 2.87 1056.13

West & East

STATION

+5.2 +2.9 +2.6 +0.8 1060.4 0.4 -0.9 9.0 -0.8 ✓
4.2 6.5 6.8 8.6 9.8 10.3 9.4 10.2 SW 1/4
60 40 30 15 9.4 15 30 40 50

+1.3 +3.5 +1.1 +0.6 1053.5 +0.7 +1.0 +0.9 +2.7 +1.7 ✓
E. bank 4.9 2.7 5.1 5.6 5.5 5.2 5.3 3.5 4.5 ✓
Stream 55 40 30 20 6.2 15 30 40 50 60

S. Bank 0.8 1053.1
Creek 7.4 6.6
1053.5
Spk. W.S.H.2
6.2 (El. = 1051.65) (Water surface at & near)
8.05 Surface H₂O
1049.4 } Creek-bed
10.3 - } In & Creek

2 Spk = NW Root 36" Maple
50' N. of Creek

B.M. EL. = 1055.66
-0.8 -0.4 -0.7 -0.1 1054.9 +0.5 +0.7 +1.2 +1.1 ✓
5.5 5.1 5.4 4.8 4.2 3.6 3.5 3.6 ✓
60 50 30 15 4.7 15 30 40 60
+1.0 +0.7 +0.4 1053.4 0.3 +1.8 +2.7 ✓
4.7 5.0 5.3 5.4 3.9 3.0 ✓
50 40 20 5.7 25 40 50

+1.7 +1.6 +0.8 +0.4 1053.6 +0.5 +2.2 +2.7 +2.8 ✓
11.1 11.2 12.0 12.4 12.3 10.6 10.1 10.0 ✓
50 40 30 15 12.8 15 30 40 50 ✓
-1.8 -1.8 -1.4 -1.2 -0.7 1056.7 -0.3 +0.5 +1.0 +1.6 +0.7 ✓
11.5 11.5 11.1 10.9 10.4 10.0 9.5 8.9 8.1 7.0 ✓
60 50 40 30 15 9.7 15 30 40 50 60 ✓
-3.7 -2.6 -2.0 -0.5 1063.9 1.4 1.1 +0.7 ✓
6.2 5.1 4.5 3.0 1.4 1.4 1.8 ✓
50 40 30 15 2.5 15 35 45 ✓

92 BLISS JUNE 11, 1928 (continued)
 ROOT
 STARK IN SILVERCREEK ROAD

STA. B.S. H.I. F.S. ELEV.
 B.M.#6 11.59 1067.25 1055.66

T.P. 10.81 1072.95 5.11 1062.14

T.P. 12.20 1083.45 1.70 1071.25

T.P. 7.89 1088.59 2.75 1080.70

B.M.#7 3.36 1085.23 B.M.#7

West. First

STA. B.M.#6 EL. = 1055.66

47+00

$$\begin{array}{r} 3.6 \quad -2.7 \quad -1.4 \\ 6.1 \quad 5.2 \quad 3.7 \\ \hline 50 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1064.8 \quad +1.1 \quad +1.4 \quad +0.9 \\ 1.7 \quad 1.1 \quad 1.6 \\ \hline 20 \quad 40 \quad 60 \end{array}$$

47+40

$$\begin{array}{r} -3.2 \quad -1.6 \\ 5.5 \quad 3.7 \\ \hline 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1065.0 \quad +0.2 \\ 2.1 \quad 1.8 \\ \hline 20 \quad 38 \end{array}$$

$$\begin{array}{r} +0.5 \\ 1.8 \end{array}$$

47+95

$$\begin{array}{r} -2.1 \quad -1.1 \quad -0.1 \\ 14.3 \quad 13.3 \quad 12.3 \\ \hline 60 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1060.8 \quad +0.2 \quad +1.2 \quad +2.0 \\ 12.0 \quad 11.0 \quad 10.2 \\ \hline 20 \quad 40 \quad 55 \end{array}$$

48+50

$$\begin{array}{r} -5.5 \quad -4.1 \\ 16.0 \quad 14.6 \\ \hline 60 \quad 40 \end{array}$$

$$\begin{array}{r} 1062.5 \quad +1.8 \quad +2.9 \\ 8.7 \quad 1.6 \quad 6.0 \quad +4.5 \\ \hline 20 \quad 35 \quad 50 \end{array}$$

49+00

$$\begin{array}{r} -5.6 \quad -4.6 \quad -2.0 \\ 16.0 \quad 15.0 \quad 12.4 \\ \hline 60 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1062.6 \quad +1.9 \quad +3.0 \quad +3.9 \\ 7.5 \quad 1.4 \quad 6.1 \quad +3.9 \\ \hline 20 \quad 44 \quad 60 \end{array}$$

49+40

$$\begin{array}{r} -5.2 \quad -3.0 \\ 15.9 \quad 10.1 \\ \hline 60 \quad 40 \end{array}$$

$$\begin{array}{r} 1065.3 \quad +0.8 \quad +1.9 \quad +2.5 \\ 6.9 \quad 5.8 \quad 5.2 \\ \hline 20 \quad 40 \quad 60 \end{array}$$

50+00

$$\begin{array}{r} -6.9 \quad -4.4 \quad -1.5 \\ 16.7 \quad 14.3 \quad 11.4 \\ \hline 60 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1073.6 \quad +1.3 \quad +1.8 \quad +1.7 \\ 8.6 \quad 8.1 \quad 8.2 \\ \hline 20 \quad 40 \quad 60 \end{array}$$

50+50

$$\begin{array}{r} -5.3 \quad -2.9 \quad -0.8 \\ 11.5 \quad 7.1 \quad 7.0 \\ \hline 60 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1077.3 \quad 0 \quad -0.5 \quad -1.4 \\ 6.2 \quad 6.7 \quad 7.6 \\ \hline 20 \quad 40 \quad 60 \end{array}$$

51+00

$$\begin{array}{r} -0.6 \quad +0.5 \quad -0.2 \\ 11.1 \quad 4.1 \quad 4.1 \\ \hline 60 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1079.0 \quad -1.0 \quad -2.6 \quad -4.0 \\ 5.5 \quad 1.1 \quad 8.5 \quad 4.0 \\ \hline 20 \quad 40 \quad 60 \end{array}$$

51+50

$$\begin{array}{r} +3.8 \quad +2.5 \quad +0.7 \\ 11.1 \quad 5.0 \quad 4.1 \\ \hline 60 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1077.8 \quad +2.4 \quad 8.2 \quad 9.4 \quad 4.2 \\ 5.7 \quad -1.4 \quad 2.5 \quad 9.4 \quad 4.2 \\ \hline 20 \quad 40 \quad 60 \end{array}$$

52+00

$$\begin{array}{r} +4.4 \quad +1.8 \\ 5.2 \quad 4.1 \\ \hline 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1073.9 \quad 2.2 \quad 15.6 \quad 15.9 \quad 6.1 \\ 1.8 \quad 1.8 \quad 75.6 \quad 50 \\ \hline 20 \quad 9.6 \quad 15 \end{array}$$

B.M.#7 EL. = 1085.22

52+30

$$\begin{array}{r} +8.8 \quad +6.1 \quad +3.3 \\ 8.6 \quad 11.3 \quad 14.1 \\ \hline 50 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1071.2 \quad -1.4 \quad -2.5 \quad -2.4 \\ 18.6 \quad 14.1 \quad 19.6 \\ \hline 20 \quad 40 \quad 60 \end{array}$$

52+60

$$\begin{array}{r} +8.1 \quad +4.7 \quad +1.8 \\ 5.2 \quad 8.6 \quad 11.8 \\ \hline 60 \quad 40 \quad 20 \end{array}$$

$$\begin{array}{r} 1075.3 \quad 3.9 \quad 14.2 \quad 14.9 \\ 13.3 \quad 2.0 \quad 4.0 \quad 6.0 \\ \hline 20 \quad 3.9 \quad 4.0 \quad 6.0 \end{array}$$

$$\begin{array}{r} -0.6 \quad -0.9 \quad -1.6 \end{array}$$

SWALE TO EAST OF ROAD

SILVERCREEK ROAD

STA.	B.S.	H.I.	ES.	ELEV.
------	------	------	-----	-------

T.P.	12.69	1089.26	12.01	1076.57
------	-------	---------	-------	---------

T.P.	11.95	1093.49	7.72	1081.54
------	-------	---------	------	---------

Q
West East

53+00	+0.3 2.0	+4.9 3.4	+3.0 5.3	1080.3 9.7	-1.4 10.3	-2.0 10.6	-2.3	✓
53+40	-4.2 2.0	+3.4 3.1	+2.2 4.3	1082.1 6.1	-1.7 1.9	-2.8 -2.8	+3.0 -3.0	✓
54+00	+3.5 6.3	+2.6 1.2	+1.2 8.6	1078.8 10.2	-0.4 7.8	-0.7 4.0	5.0 6.0	✓
54+40	+2.3 8.2	+1.6 4.1	+0.3 10.4	1077.9 12.5	-1.8 10.7	+3.2 2.0	15.7 5.0	✓
54+65				1076.6 12.0	-3.1 2.0	17.5 40	5.4	← Bottom Gully

55+00	+0.2 15.7	+0.1 15.8	+0.5 15.4	1073.4 17.0	+1.1 15.9	+0.2 18.2	+1.1 5.0	✓
55+20				1073.3 15.7	+0.3 15.4	+0.9 13.6	+2.4 13.7	✓
56+00	-1.4 6.0	-0.6 4.0	-0.6 2.0	1080.1 8.3	+0.9 1.2	+1.2 4.0	+1.3 7.9	✓
56+60	-1.0 6.0	-0.1 4.0	+0.3 2.0	1087.0 2.4	-0.6 2.4	-1.5 3.8	5.2 3.0	✓
57+00	+1.7 6.0	+2.4 3.1	+1.5 11.5	1086.6 2.7	-2.1 2.0	3.6 4.0	7.2 6.0	✓

57+60	+3.8 6.1	+3.1 6.8	+1.7 8.1	1083.6 10.5	+0.9 11.9	-2.0 11.9	-2.3 12.2	✓
58+00	+2.3 6.0	+2.0 4.0	+0.8 2.0	1084.0 9.5	-0.6 2.0	7.5 5.0	10.6 5.2	← Edge Bank
58+70	+2.8 6.0	+1.9 4.0	+0.3 2.0	1086.4 7.1				✓
59+00	+1.4 6.0	+9.3 3.0	+8.3 6.0	1079.2 14.3				✓
+38	+6.6 2.0	+4.8 1.0	+4.0 5.4	1084.1 9.4				✓
+50	+10.0 5.5	+8.3 4.0	+5.6 2.0	1079.2 14.3				✓

STA.	B.S.	H.I.	F.S.	ELEV.
	6.06	1094.02	5.53	1087.96

South Edge Pavement.

11.84 1082.18

B.M. 5.15 1087.31 1082.16

West East

59+60	+5.3 3.3	+3.8 4.8	+1.8 6.3	1085.4	✓
59+80	+5.6 3.1	+4.0 4.4	+2.4 6.3	1085.3	✓
60+00	+8.8 2.8	+6.9 6.3	+5.3 6.3	1082.4	✓
+35	+11.3 1.1	+8.8 4.5	+6.9 6.2	1080.9	✓
+60	+7.1 1.1	+5.5 2.7	+3.5 4.1	1085.8	✓
61+00	+5.7 0.5	+4.4 1.0	+2.3 3.1	1087.8 -2.4 -4.5 10.7	✓ -9.0 15.2
61+50	+3.2 4.0	+1.9 2.0	+2.1 3.7	1090.3 -2.0 5.8	✓ =4.4 10-6.7
61+60	+1.2 0.1		+1.7 3.7	1091.9 1.7	✓

B.M. on culvert on pavement El. 1082.16

Repeat 58+70	1086.4	-17.4	-17.9	18.3	18.8	✓
59+00	1079.1	-9.9	18.6	18.6	✓	
59+38	1083.5	-10.0	-13.3	13.8	13.3	✓
59+50 Not taken	1083.9	-2.9	-14.6	-15.1	18.5	✓
59+60	1086.5	+16.7	17.2	16.0	✓	
59+80	1083.0	-13.0	12.3	17-13.4	✓	
60+00	1081.1	-10.0	-11.2	17.2	11.0	✓
60+35	1086.4	+14.3	12.6	16.8	✓	
60+60	0.9	2.2	4.0	6.0	-15.9	✓

98 Elevations - Russell Farms

B.S.	H.L.	F.S.	Elev
B.M.	5.15	1087.31	1082.16
		13.8	1073.5
		19.4	1067.9
		14.8	1072.5
		3.33	1084.0

C.W. Courtney's B.M. = 459.91
 U.S.G.S. Elev. same B.M. = 1085.34
 Diff in Datum = 625.43

E1. = 1082.16

B.M. on Culvert - N-Side Road

Top Box - Culvert at foot of hill

* Bottom " - " " " " "

W. Bank Creek 15' South Culvert

Center of pavement at Culvert

100 Russell Farms 11/2/28 E. P. F. S. E. P. S.
B.S. H.I. ✓ F.S. Elev

B.M. #6 9.27 1064.93 1055.66

Ground ✓ 10.1 54.8

T.P. 3.60 63.25 5.28 59.65 ✓

B.M. ✓ 4.90 58.35

along
E. Dam 0.59 58.94 58.35

0+00 ✓ 1.2 57.7

0-50 +3.0 ± 61.9

0+40 10.5 48.4

1+00 12.9 46.0

1+55 12.4 46.5

14.0 44.9

14.3 44.6

1+85 10.6 48.3

2+00 11.6 47.3

3+00 11.4 47.5

3+65 9.6 49.3

4+00 4.1 54.8

4+12 0.8 58.1

4+60 +5 ± 64.
13.1 45.8
15.6 43.3

Toe bank 300± W. of RD & +200 S. of fence

High pt on flat white granite boulder, 200± E. of
(12 ft E. of N. end dam)
N. prop. line + 100± N. of creek (near small
sycamore trees)
0+00 = N. end

50± trees to grub
+ lots of brush.

N. bank creek
surface H₂O
bottom creek
S. bank creek

→ Creek bank at W. prop line
surface H₂O at W. prop line

Levels for John Hinckley & Harry Fisher along Silver Creek

102
on old Fisher farm in Russell Twp 3/30/29

B.M. #	BS	HI	FS.	Assumed
6.10	106.10			100.0
		9.6	96.5	
		8.12	97.98	
		2.7	103.4	
		5.1	101.0	
		5.0	101.1	
T.P.	2.91	104.16	4.85	101.25
			4.18	99.98
			1.10	103.06
			0.91	103.25
			1.36?	102.80
B.M. #2			2.17	101.99

B.M. #1	6.49	106.49	100.00
		6.51	99.98

Sp. W. side 15" Willow 16ft W. of E. ^{prop fence} line, 200ft N of Channel.
 Bot. Channel at E prop line fence
 Top H₂O " " " " "
 Top bank & natural ground ^{South side creek} at E. prop line fence
 Ground 150ft North main Channel at E. prop line
 " 50 " " " " " " " "

Several stakes set around edge proposed lake
 North End high part old ^{dam} embankment
 Middle " " " "
 South End " " " "
 Spike N. side E. foot 36 Elm E. toe steep bank 800ft from Rd.

Auburn Center — Chardon Center

STA	BS	HI	FS	Elev.
BM	4.89	1253.63 1272.715		1263.74 1262.225
TP	7.83	1281.52 1270.63	0.935	1272.67 1271.780
D.O			6.25	1275.27 1274.37
			5.44	1276.99 1276.09
2 TP	6.80	1295.11 1284.52	2.91	1292.61 1277.72
3			3.9	181.5
6			4.9	80.5
TP	6.63	1286.65 1285.76	5.29	1291.12 1279.23
11				
TP	2.05	1282.43 1291.54	6.27	1280.38 1279.49
16721				
TP	4.67	1289.55 1288.86	2.35	1280.08 1279.19
21			6.8	1282.95
TP & BM	11.20	1285.42 1294.53	5.63	1284.22 1283.73
TP	8.58	1301.75 1300.39	2.23	1293.14 1292.30
22			11.00	1290.77
TP	10.60	1311.31 1310.42	1.06	1300.71 1299.82
23			10.2	1301.1

Road May 5 1929

W E E

On 36" Sexamora Tree West of Huff House

Elev. 1275.13 from Blum

6.25 N. Edge Pavement

On N.W. corner Cone Hill wall

2.91

3.95

4.96

3.25

5.16 TOP culvert barrel

6.8	6.6	7.90	6.80	7.4	6.60	5.80
30	15	10	10	10	15	30

Close to 2 Steel Leg
 on cone Base to ~~2~~ Leg C.E.I. Tower No 20119

6.80	D.10	12.3	11.00	11.80	9.15	6.80
30	15	10	10	10	15	30

9.30	5.40	16.50	11.60	9.50	9.30
30	15	12	10	16	30

106	B5	H1	F5	EL
24		1311.31	6.0	1305.3
25			8.60	1302.7
TP	1.05	1306.01 1305.42	5.55	1305.76 1304.85
26			7.80	1299.0
27			7.0	1299.8
30			4.10	1302.7
TP	6.51	1310.58 1309.64	2.74	1304.05 1303.18
36			3.0	1307.6
TP	3.06	1308.44 1307.60	5.14	1305.44 1294.55
40			6.0	1302.5
42+34			4.2	1304.3
44			11.10	1297.4
TP	1.14	1292.14 1292.25	11.49	1297.00 1296.11
TP BM	3.03	1291.33 1290.64	9.64	1288.50 1287.61
48			6.2	1285.3
TP	0.58	1282.12 1281.53	9.64	1281.74 1280.95
50			7.0	1275.4
TP	2.00	1275.44 1274.60	8.93	1273.44 1272.60
51			8.7	1266.8

W		E			107	
$\frac{5.20}{30}$	$\frac{5.20}{12}$	$\frac{2.00}{10}$	6.00	$\frac{2.00}{11}$	$\frac{4.50}{15}$	$\frac{4.20}{30}$
$\frac{9.70}{30}$	$\frac{2.20}{15}$	$\frac{9.80}{12}$	8.60	$\frac{9.70}{9}$	$\frac{6.50}{16}$	$\frac{5.80}{30}$
	$\frac{8.20}{20}$		2.80	$\frac{8.85}{20}$		
$\frac{5.80}{20}$	$\frac{6.2}{14}$	$\frac{8.60}{10}$	2.00	$\frac{8.0}{20}$	$\frac{5.40}{20}$	
			4.10			
			3.0			
TOP OF Large Stone 20' RT 344.80						
			6.0			
	$\frac{4.40}{20}$		4.20	$\frac{2.50}{20}$	20' Extreme TOP of 1+11	
	$\frac{10.70}{30}$		11.10	$\frac{10.10}{20}$		
On Large Stone 41 30. of E Face Part 25' Left of 47+00						
$\frac{5.50}{30}$	$\frac{6.30}{10}$	$\frac{2.0}{7}$	6.20	$\frac{7.60}{11}$	$\frac{4.60}{12}$	$\frac{3.60}{30}$
$\frac{3.70}{30}$	$\frac{3.30}{11}$	$\frac{8.40}{6}$	7.60	$\frac{6.70}{10}$	$\frac{8.80}{15}$	$\frac{4.3}{19}$
						$\frac{2.60}{30}$
$\frac{3.30}{30}$	$\frac{3.40}{12}$	$\frac{4.30}{6}$	8.70	$\frac{8.40}{13}$	$\frac{10.30}{15}$	$\frac{3.70}{22}$
						$\frac{3.60}{30}$

	B 3	H 1	F 5	E 6
TP	0.34	1265.20 1264.31	10.63	1264.86 1263.92
52			9.0	1256.2
52+50			11.9	1253.3
TP	5.21	1260.67 1259.78	9.74	1255.46 1254.57
54			10.5	1250.2
54+65			8.9	1251.8
TP+BM	11.63	1250.33 1249.44	1.97	1259.70 1258.81
56			8.7	1261.6
TP	10.21	1258.50 1257.61	1.84	1268.49 1267.60
58			6.5	1272.2
59			3.9	1274.8
60+33.2			1.9	1276.8
TP	0.75	1272.06 1271.17	7.39	1271.31 1270.42
62			2.8	1269.3
64			11.9	1260.2
TP	1.19	1262.28 1262.39	9.95	1262.09 1261.20
65			11.10	1252.2
TP	8.22	1258.56 1257.67	12.94	1250.34 1249.45
66			10.7	1247.9

3.70 30	5.40 14	9.5 6.0	4.00	9.0 11	9.80 14	4.60 21	5.20 30
11.3 30	10.5 15	12.5 50	11.90	12.10 10	11.20 20	9.90 30	
			10.50				
7.10 30	5.60 23	9.30 10	8.90	10.00 10	9.10 75	4.20 25	Now stump 11/150
8.50 30	7.50 13	10.40 9	8.70	10.6 12	6.40 20	4.150 30	1 1/2 UP N Hill
7.60 30	6.20 12	8.00 9	6.60	7.20 13	4.60 16	2.80 30	
6.00 30	4.10 10	5.0 8	3.50	4.40 11	2.20 20	1.20 30	
			1.90				
3.60 30	3.10 10	4.20 8	2.80	4.40 12	1.00 18	0.40 30	
10.0 30	10.9 10	13.5 7	11.9	14.2 14	10.8 17	10.0 30	
8.50 30	10.0 10	12.6 6	11.10	13.10 11	9.10 13	6.80 30	
13.6 30	11.9 10	12.6 8	11.70	11.60 12	11.00 14	12.60 30	

	BS	HT	FS	EL
TP+BM	7.16	1257.56 1267.67	7.16	1251.41 1250.52
67+60			8.1	1250.5
67+00			4.0	1254.6
TP	12.22	1267.78 1267.79	2.06	1256.50 1255.61
69			4.9	1263.9
TP	9.77	1275.77 1274.99	2.67	1266.70 1266.21
69+60			8.0	1267.9
70			7.6	1268.3
TP	9.97	1272.60 1271.71	3.26	1272.62 1271.73
71			11.9	1270.7
72			5.3	1277.3
TP	10.17	1290.78 1289.89	1.99	1280.61 1279.72
73			6.5	1284.3
TP+BM	7.11	1290.78 1289.89	7.11	1283.67 1282.78
75			5.9	1284.9
TP	0.84	1284.36 1283.47	7.31	1283.47 1282.58
77			3.2	1281.2
74			3.9	1280.5

	in Creek	on W. Hill	in Creek
	16.70	11.2	16.70
	40 ft W of Sta 66+70		
	on Blue Stone with Red Knobs		on Top Knop
	$\frac{11.20}{30}$	$\frac{9.30}{9}$	$\frac{9.30}{15}$
	$\frac{2.30}{30}$	$\frac{1.40}{10}$	$\frac{4.90}{18}$
	$\frac{2.50}{30}$	$\frac{5.70}{4}$	$\frac{2.20}{22}$
	$\frac{8.0}{30}$	$\frac{6.50}{12}$	$\frac{8.80}{15}$
		8.80	$\frac{5.10}{25}$
		8.80	$\frac{3.70}{30}$
		8.80	$\frac{2.60}{18}$
		13.50	$\frac{12.90}{18}$
		11.40	$\frac{10.70}{30}$
		5.30	$\frac{2.10}{30}$
		6.60	$\frac{5.30}{18}$
		6.60	$\frac{4.40}{30}$
		5.90	
		3.20	
		3.90	

on Red Boulder 100 ft W of Sta 73+00

Sta	BS	HI	FS	EL
83		1284.36	1.5	1282.9
TP	842	1288.79 1287.90	0.99	1283.30 1282.48
			3.22	1285.57
				1284.35
BM			4.44	1283.46
				1284.37

BM 1270.13

Q
- 1.50

3.22 so edge pavement
 2 nails in NE Root 40" Elm stump 100' so of King Hwy
 Gone

Nail S root 48" Chestnut ± 2000
 NWly on N side King Memorial
 just north of CE 1 pole
 # 551671

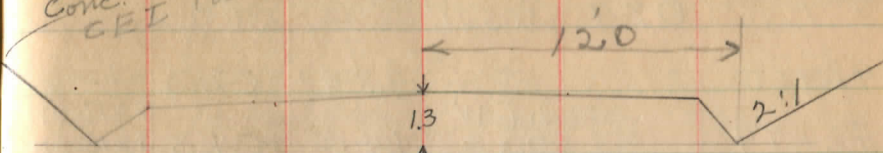
5/22/29 Chardon-Auburn Center Rd
FRZ & C.L. Bliss

B.M.	9.79	1294.01		1284.22	
22+00			2.8¢	91.2	
T.P.	11.04	1304.65	040	1293.61	
22+00			13.4¢	91.2	
22+00			9.6 E		S=22.0
			9.9 W		S=22.0
22+00			1.2 W		S=20.0
23+00			1.1 E	01.3	S=20.0
T.P.	5.80	1309.0	1.45	1303.20	
23+50			4.8¢	04.2	
24+00			2.4 E		S=20.0 E
			2.7 W	05.4	S=20.0 W
25+00			4.1 E		S=18.0 E
			5.3 W	03.0	S=16.0 W
T.P.	5.62	07.25	7.37	01.63	
28+00			7.2¢	00.0	
29+00			4.1¢	03.1	
30+00			4.8¢	02.4	
B.M.			4.59	1302.66	

Conc. Base / Leg
CEI Tower

¢

115



Note: Slope stakes set back 3'-00" from top of slope to be and Rdgs in last col.

cut ¢ 0.0

cut ¢ 0.5

cut West side

East side

$\frac{4.0}{25}$	$\frac{3.6}{15}$	$\frac{6.5}{12.5}$	$\frac{5.5}{9}$	4.8 ✓	$\frac{5.3}{7}$	$\frac{6.2}{9.5}$	$\frac{3.1}{14}$	$\frac{2.6}{25}$
------------------	------------------	--------------------	-----------------	-------	-----------------	-------------------	------------------	------------------

cut ¢ 2.0

cut ¢ 0.0

$\frac{6.7}{20}$	$\frac{6.3}{15}$	$\frac{6.5}{14}$	$\frac{8.9}{12}$	$\frac{7.7}{8.72}$	$\frac{7.9}{9}$	$\frac{8.5}{12}$	$\frac{6.1}{16}$	$\frac{5.7}{20}$	$\frac{5.6}{25}$
$\frac{4.0}{25}$	$\frac{3.9}{20}$	$\frac{4.0}{14}$	$\frac{6.4}{12}$	$\frac{5.1}{8}$	4.1 ✓	$\frac{5.1}{10}$	$\frac{6.2}{13}$	$\frac{3.1}{18}$	$\frac{2.7}{25}$
$\frac{5.4}{20}$	$\frac{5.9}{12}$	$\frac{6.6}{10}$	$\frac{5.7}{8}$	4.8 ✓		$\frac{5.9}{14}$	$\frac{4.7}{15}$	$\frac{5.1}{20}$	$\frac{4.8}{25}$

Spt on S. root 30" Elm 30 West 29+90

5/22/29 Chard-Auburn RD

T.P. ^(B.M.) 0.27 1305.71 1305.44

42+00 Rd 3.4¢ 02.3

42+79 1.6 W 1.4¢ 04.3 S=16.0W
0.3 E S=18.0E

43+00 2.2¢ 03.5

43+50 6.0¢ 99.7

T.P. 1.14 1298.80 8.05 1297.66

10.25 1288.55 1288.50

B.M. 6.00 1289.67 1283.67

74+00 3.8 E 4.2 W 3.8¢ 85.9 S=15.0 E S=15.0 W

73+50 3.4 E 3.6 W 3.8¢ 85.9 S=18 E S=17 W

73+00 4.2 E 4.2 W 5.3¢ 84.4 S=19 E S=19 W

72+00 9.2 E 8.1 W 12.2¢ 77.5 S=20 E S=22 W

T.P. 0.16 1278.49 11.34 1278.33

71+00 2.0 W 8.0¢ 70.5 S=24 W

70+00 10.2¢ 68.3

69+50 9.5 W 10.9¢ 67.6 S=19.0 W

T.P. 0.02 67.99 10.52 67.97

West

East 117

Top large Stone 20' Rd. (E) 39+80

Cut = 0.0 $\frac{4.2}{25} \frac{4.1}{9} \frac{4.7}{10} 3.4$ ✓ $\frac{4.4}{9} \frac{3.2}{11} \frac{1.9}{25}$

cut $\phi = 1.0$ $\frac{2.0}{25} \frac{1.6}{20} \frac{2.0}{13} \frac{3.9}{10} \frac{3.1}{8} 2.2$ ✓ $\frac{1.5}{9} \frac{2.0}{10} \frac{0.5}{2} \frac{0.0}{20} + \frac{0.5}{25}$

? $\frac{2.0}{25} \frac{1.6}{20} \frac{2.0}{13} \frac{3.9}{10} \frac{3.1}{8} 2.2$ ✓ $\frac{2.8}{7} \frac{3.0}{10} \frac{1.0}{13} + \frac{0.5}{25}$

$\frac{4.9}{25} \frac{4.9}{12} \frac{7.4}{9} \frac{6.8}{7} 6.0$ ✓ $\frac{6.6}{7} \frac{7.7}{10} \frac{5.4}{13} \frac{4.2}{25}$

on Red boulder 100' W. of 73+00

Cut $\phi = 0.0$ $\frac{4.1}{25} \frac{4.3}{11} \frac{5.0}{10} 3.8$ ✓ $\frac{4.8}{13} \frac{3.9}{15} \frac{3.4}{25}$

cut $\phi = 1.0$ $\frac{3.5}{25} \frac{3.7}{11} \frac{4.8}{10} 3.8$ ✓ $\frac{4.4}{12} \frac{5.0}{15} \frac{3.7}{17} \frac{2.9}{25}$

cut $\phi = 1.0$

cut 0.0

cut 0.0

cut 0.0

cut 1.0

922/29	1267.99				S=20.E
69+00	2.2E 1.4W	3.9¢	64.1		S=22W
68+00	11.3W	13.4¢	54.6		S=18W
T.P.	1.59	56.50	13.08	54.91	
B.M.		5.00	51.50	1251.41	
T.P.	12.61	1266.65	246	54.04	
64+50	8.2W 8.0E	10.6¢	56.0		S=20W S=20E
64+00	4.7W 5.1E	6.6¢	60.0		S=20W S=20E
63+00	1.3W 0.0E	1.6¢	65.0		S=15W S=18.0E

West East 119

ent¢=1.0

ent¢=0.0

cur¢=0.0 $\frac{8.3}{2.5} \frac{9.1}{9} \frac{11.4}{6}$ 10.6 $\frac{11.0}{11} \frac{12.2}{14} \frac{8.5}{18} \frac{7.5}{2.5}$

ent¢=1.0

cur¢=0.0 $\frac{13}{20} \frac{16}{9} \frac{30}{7} \frac{21}{5}$ 1.6 $\frac{2.0}{12} \frac{2.9}{14} \frac{0.0}{20}$

ent 0.0 } 59

" 1.5 } 60

ent 2.3 } 60+33

" 0.0 } 61+00

5/23/29 Chardon-Auburn Center Rd.

B.M.	12.60	1271.30		1258.70
T.P.	9.28	1280.25	0.33	1270.97
59+00	6.1 W 4.2 E	5.4		1274.8
60+00	4.6 W 1.4 E	3.1		77.15
B.M. ^{5/23}		5.83		1274.42
60+70	4.5 W 1.9 E	3.3		76.95
61+50	8.0 W 5.9 E	8.6		71.65

F.F.Z. G.L.B.
H. Clause
West & East
Bent Spk 71. root 15" Cherry 25' W 55+00

cut 0.0	$\frac{7.0}{2.5}$	$\frac{5.7}{9}$	$\frac{6.6}{7.5}$	5.4	$\frac{6.4}{12}$	$\frac{4.2}{16}$	$\frac{3.5}{2.5}$
cut 1.5	$\frac{5.5}{2.5}$	$\frac{4.4}{9}$	$\frac{4.7}{8}$	3.1	$\frac{3.7}{12}$	$\frac{1.6}{17}$	$\frac{0.9}{2.5}$
bent Spk 38' W	Sta 59+65 in E. root 12" Maple						
cut 2.0	$\frac{5.7}{2.5}$	$\frac{4.7}{20}$	$\frac{4.5}{10}$	$\frac{5.6}{8}$	3.3	$\frac{5.1}{14}$	$\frac{2.4}{18}$
cut 0.0	$\frac{8.5}{2.5}$	$\frac{8.0}{9}$	$\frac{9.7}{7}$	8.6	$\frac{9.8}{15}$	$\frac{5.9}{20}$	$\frac{5.4}{2.5}$

7/31/29	C L B	#	Cloues	FS	FL
BM	2.10		1290.60		1288.50
TP	2.07		1285.46	7.31	1283.29
49			3.3 W 3.2 E	4.0	81.5
50			0.3 W 8.2 E	10.0	
TP	2.45		1275.48	12.43	1273.03
51			3.0 W 9.2	9.20	
TP	9.95		1274.15	1.28	1274.20
50			5.0 W 5.3 E	8.70	
TP	9.64		1291.61	2.18	1291.97
BM				3.02	1288.59

6/3/29 FRZ
H Clause cold

B.M.	7.96	1284.95	7.96	1276.99
Int. #85			8.68	1276.27
1+00			7.5	77.45
2+00			5.4	79.55
3+00			2.7	82.25
4+00			2.6	82.35
5+00			3.5	81.45
6+00			3.6	81.35
7+00			3.6	81.35

West East 123
On Stone 5' 30" of Fence Post 25' L of Sta 47+00

$$\text{cut } \phi = 0.0 \frac{3.1}{30} \frac{3.3}{20} \frac{3.5}{8} \frac{4.8}{6} \frac{4.2}{4} 4.0 \frac{4.6}{15} \frac{5.3}{16} \frac{3.2}{18} \frac{1.5}{25} \frac{0.6}{30}$$

$$\text{cut } \phi = 1.0$$

$$\text{cut } \phi = 0$$

$$\text{cut } \phi = 0-00$$

$$\text{cut } \phi = 1.0$$

N.W. & Conc. Hed w/ Sta. 0+10

$\frac{6.9}{25}$	$\frac{7.5}{17}$	$\frac{9.2}{15}$	$\frac{8.2}{10}$	7.5	$\frac{8.1}{10}$	$\frac{9.3}{12}$	$\frac{8.0}{15}$	$\frac{6.8}{25}$
$\frac{4.3}{25}$	$\frac{4.4}{15}$	$\frac{6.8}{13}$	$\frac{5.7}{10}$	5.4	$\frac{5.7}{10}$	$\frac{7.1}{12}$	$\frac{5.7}{15}$	$\frac{5.4}{20}$
$\frac{2.1}{25}$	$\frac{2.5}{17}$	$\frac{4.3}{15}$	$\frac{3.0}{12}$	2.7	$\frac{3.1}{10}$	$\frac{5.0}{12}$	$\frac{3.3}{15}$	$\frac{3.2}{25}$
$\frac{2.0}{25}$	$\frac{2.7}{15}$	$\frac{4.2}{15}$	$\frac{3.4}{10}$	2.6	$\frac{3.1}{10}$	$\frac{4.2}{12}$	$\frac{3.1}{15}$	$\frac{2.3}{25}$
$\frac{3.8}{25}$	$\frac{4.0}{15}$	$\frac{5.3}{13}$	$\frac{4.1}{10}$	3.5	$\frac{3.6}{10}$	$\frac{5.3}{13}$	$\frac{3.7}{15}$	$\frac{3.2}{25}$
$\frac{3.7}{25}$	$\frac{4.2}{15}$	$\frac{5.3}{13}$	$\frac{4.0}{10}$	3.6	$\frac{4.2}{10}$	$\frac{4.9}{13}$	$\frac{3.7}{15}$	$\frac{2.9}{25}$
$\frac{4.0}{25}$	$\frac{4.0}{17}$	$\frac{4.5}{15}$	$\frac{4.1}{13}$	3.6	$\frac{3.9}{10}$	$\frac{5.1}{12}$	$\frac{4.4}{15}$	$\frac{4.5}{25}$

Chardon-Auburn Center Road

X Secs After Grading

BS MI FS

BM	9.38	1296.35		1296.49
1 ✓			28.80	77.6
2 ✓			26.9	79.5
3 ✓			25.1	81.3
4 ✓			24.2	82.2
5 ✓			24.6	81.8
6 ✓			24.5	81.9
7 ✓			24	82.5

BM 1304 1297.26 1297.22

22 ✓			24.5	92.6
TP	1269	1302.17	2.78	1294.18
23 ✓			6.9	1300.3
23+50 ✓			4.1	1303.1
TP	4.64	1304.34	2.52	1304.65
24 ✓			4.9	04.4
25 ✓			6.1	03.2

125
6/15/29

June 15 1929

Chardon
H.C.

West

East

On NW 4 cone. Hdwall

$\frac{9.0}{15}$	$\frac{10.2}{13}$	$\frac{9.2}{10}$	8.80	$\frac{9.7}{10}$	$\frac{10.23}{13}$	$\frac{9.11}{16}$
$\frac{5.3}{13}$	$\frac{8.5}{14}$	$\frac{6.7}{10}$	6.4	$\frac{7.0}{10}$	$\frac{8.5}{13}$	$\frac{7.7}{16}$
$\frac{3.9}{16}$	$\frac{6.5}{13}$	$\frac{5.2}{10}$	5.1	$\frac{5.3}{10}$	$\frac{6.7}{13}$	$\frac{4.6}{16}$
$\frac{4.2}{16}$	$\frac{6.0}{13}$	$\frac{4.5}{10}$	4.2	$\frac{4.9}{10}$	$\frac{6.2}{13}$	$\frac{4.4}{16}$
$\frac{5.5}{16}$	$\frac{6.8}{13}$	$\frac{4.8}{10}$	4.6	$\frac{5.0}{10}$	$\frac{6.6}{13}$	$\frac{5.1}{16}$
$\frac{5.6}{16}$	$\frac{6.5}{13}$	$\frac{4.7}{10}$	4.5	$\frac{4.7}{10}$	$\frac{6.8}{13}$	$\frac{5.1}{16}$
$\frac{5.4}{16}$	$\frac{6.3}{13}$	$\frac{4.7}{10}$	3.9	$\frac{4.6}{10}$	$\frac{6.6}{13}$	$\frac{5.8}{16}$

cone Base N 4 y P E / Tower

$\frac{2.3}{25}$	$\frac{6.6}{13}$	$\frac{4.8}{10}$	4.7	$\frac{5.7}{10}$	$\frac{6.9}{10}$	$\frac{2.3}{21}$
$\frac{3.8}{22}$	$\frac{2.5}{15}$	$\frac{2.3}{10}$	6.8	$\frac{6.8}{5}$	$\frac{2.0}{10}$	$\frac{2.6}{2.2}$
$\frac{2.0}{27}$	$\frac{5.8}{13}$	$\frac{4.7}{10}$	4.1	$\frac{4.0}{10}$	$\frac{5.0}{13}$	$\frac{1.2}{2.7}$
$\frac{3.5}{22}$	$\frac{7.0}{13}$	$\frac{5.6}{10}$	4.9	$\frac{5.3}{10}$	$\frac{6.5}{15}$	$\frac{2.6}{2.2}$
$\frac{5.8}{18}$	$\frac{8.2}{13}$	$\frac{7.2}{10}$	6.1	$\frac{6.4}{50}$	$\frac{7.7}{10}$	$\frac{4.5}{2.0}$

	B.S.	130934 HI	F.S.	EL.
TP	545	1302.95	684	1302.50
28 ✓			479	1300.05
29 ✓			648	03.15
30 ✓			451	02.85
BM			5.26	1302.69

FR2
1302.66

TP (BM)	205	1302.79	2.05	1305.44
42 ✓			4.7	02.8
42+79 ✓			4.1	03.4
43+00 ✓			4.5	02.8
43+50 ✓			7.2	1300.3
TP	0.66	1297.52	10.62	1296.87

1297.50

TP BM	1.36	1289.89	9.0	1288.52
49 ✓			4.40	85.5
49 ✓			8.20	81.7
TP	2.46	1280.63	11.67	1278.21
50 ✓			5.5	75.2
TP	2.76	1272.85	10.38	1270.09
51 ✓			4.8	68.05

?

X Sec. after grading

127

West		E	East
22 15	94 13	84 10	7.9
4.7 15	6.5 13	54 10	4.8
6.4 13	7.6 13	60 10	5.1
			8.2
			9.5
			6.6
			10
			13
			16
			5.2
			6.4
			15
			19
			5.5
			6.6
			12
			16

SPOX S Root 30" E/m 30' W 29+60

TOP Large Stone 20 RT (E) 39+70

5.8 15	7.0 13	5.2 10	4.7	5.4 10	6 13	4.4 15
34 17	6.8 13	4.7 10	4.1	4.1 8	5.3 11	1.9 20
3.5 18	6.5 13	5.2 10	4.7	5.6 10	6.0 13	2.4 19
6.6 13	9.0 13	7.0 10	7.2	7.8 10	9.2 13	6.3 16

4.2 13	6.0	4.8 10	4.40	4.9 10	6.2 13	3.2 15
8.2 16	9.8 13	8.5 10	8.2	8.6 14	10.7 16	8.2 20

2.2 23	6.2 13	5.5 11	5.5	5.9 12	2.4 14	3.5 19
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1.3 19	6.0 13	4.9 10	4.8	5.2 10	7.2 14
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NO DIT MARKS

Chardon-Auburn Center Road

	BS	H1	FS	EL	
64+50 ✓		1259.01	22.11	56.6	
65 ✓			25.3	53.7	
66 ✓			10.2	48.8	
TP	BM 9.57	1260.98	7.0	1251.41	1251.41
67+50 ✓			28.7	52.3	
68 ✓			25.4	55.6	
TP	12.03	1272.03	0.98	1260.00	
69 ✓			28.7	63.3	
69+50 ✓			25.7	66.3	
70 ✓			23.6	68.4	
TP	10.62	1282.00	0.65	1271.38	
71 ✓			29.3	72.7	
72 ✓			23.3	78.7	
TP	7.17	1288.70	0.47	1281.23	
73 ✓			25.2	83.5	
+50 ✓			23.7	85.0	
74 ✓			22.9	85.8	
BM			5.12	1283.58	1283.67

X Secs. after grading

West				East		
0.7	3.7	2.8	2.4	2.8	4.5	0.3
20	10	8		11	15	21
6.0	7.2	5.5	5.3	6.0	8.5	Bump not cut
14.5	12	4		4	14	
12.4	10.6	10.2	10.2	10.7	12.0	
11	6.0			11	15	
11	9.6	8.5	8.5	9.7	11.7	
11.1	4.6	8.5	8.5	9.2	11.2	
14	11			14	18	
4.2	2.0	5.4	5.4	6.0	2.4	
14	11	11		13	14	
5.8	10.2	4.0	8.7	9.4	10.8	
23	12	9		16	19	
3.6	6.6	5.7	5.7	6.0	2.1	
14	14	11		14	15	
7.2	2.2	4.4	3.6	3.6	5.0	3.6
12	4	4		14	15	20
6.0	10.7	4.4	4.3	10.2	12.6	
28	12	9		8	16	
0.6	5.4	3.7	3.3	4.4	5.9	1.9
21	12	9.0		12	14	21
3.4	6.4	5.4	5.2	5.2	6.2	3.4
17	12	8		5	9	20
2.8	4.4	4.2	3.7	4.5	5.4	2.3
10	13	11		10	12	20
3.5	5.0	4.0	2.9	3.5	4.8	3.2
16	14	1.2		10	12	15

on Boulder 107' W 53#00

BLISS } CHECK LEVELS - Russell Farms
 Root }
 Rod }
 STARK } JUNE 7, 1928

	B.S.	I.I.	F.S.	ELEV.
B.M.	12.00	1094.16		1082.16
B.M.			8.82	1085.34
T.P.	6.74	1092.90	8.00	1086.16
B.M.#7	1.04	1086.26	7.68	1085.22
T.P.	0.33	1074.21	12.38	1073.88
T.P.	5.16	1066.48	12.89	1061.32
B.M.#6	2.88	1058.54	10.82	1055.66
T.P.	12.25	1068.82	1.97	1056.57
T.P.	11.54	1078.69	1.67	1067.15
T.P.	12.19	1090.25	0.63	1078.06
B.M.#5	11.14	1100.64	0.75	1089.50
T.P.	10.66	1111.04	0.26	1100.38
T.P.	8.32	1118.14	1.22	1109.82
B.M.#4			2.66	1115.48

"X" on
 B.M. - S.W. Cor. N. Headwall of Culvert
 at Manchester Hill. - 3rd Tier Stones
 ← COURTNEY BENCH - Hdwl on S. Side Rd.
 "X" on S.W. Corner top stone.
 ELEVATION PER C.W.C. = 459.91

B.M.#7 - Boulder 75' W. of E. and 10'
 South 1st Wire Fence,

B.M.#6 { 2 Spikes N.W. Root 36"
 Maple - 50' N. Creek

B.M.#5 { 2 Spikes E. Root 30"
 Elm - West of Ravine

B.M.#4 2 Spikes E. Root 30"
 Maple 75' W. Sta. 36+50

Eliss
Stark
Root

PROFILE CHECK -

6/11/28

SILVERCREEK ROAD - (Russell Farms)

Page 136

	B.S.	H.I.	F.S.	ELEV
BM.#2	8.13	1172.69		1164.56
B.M. 2A			2.90	1169.79
B.M. 2F	2.63	1172.40		1169.77
			6.55	1165.85
			12.98	1159.42
T.P.	3.30	1163.57	12.13	1160.27
			5.07	1158.50
T.P.	12.28	1171.55	4.30	1159.27
			5.78	1165.77
			11.87	1159.68
T.P.	0.97	1161.56	10.96	1160.59
			6.89	1154.67
T.P.	0.74	1150.37	11.93	1149.63
			3.60	1146.77
			16.4	1133.97
			12.09	1138.28
			7.64	1142.73

137

B.M.#2 El. 1164.56[?] (Arbitrary figure)
1169.77 - BM#2A per D.R. Stark

Arb. Elev.

— NOTE —

Sta 14+00

DO NOT USE

" 12+00

FIGURES AND

COMPUTATIONS

Sta. 10+00

APPEARING ON

T.P.

PAGES 136,

T.P.

137, 138 and

T.P.

139.

T.P.

ELEVATIONS

T.P.

USED HERE ARE

T.P.

ARBITRARY

T.P.

FIGURES EMPLOYED

T.P.

FOR PURPOSES

T.P.

OF A CHECK

T.P.

ONLY,

D.R. Stark

B.S.	H.I.	F.S.	Elev.
1.97	1161.24		1159.27
		6.73	1154.51

Elev. 7+60

11.74	1177.51		1165.77
		3.77	1173.74 7+00
		3.57	1173.94 6+00
		.55?	1176.96 4+00
		4.68	1172.83 BM#1

Sta. 9+70

C Error on turn to Sta. 9+70

Sta. 7+00

6+00

4+00

See Note on page 137

140

141

24/29 F.R.Z. Levels for Joe Blacford
 H.T. on form (S. Folger) pakeel
 Chapter for possible
 assumed lake

	100.0	7.8	92.2
		10.4	89.6
		12.0	88.0
		8.5	91.5
T.P.	9.0	105.3	3.7
			96.3
			8.2
			97.1
			10.4
			94.9

12
 2
 24
 80
 1920

Dam = about 220 ft long
 of so. Prop line
 on Grd. So. side 30' Maple in Valley 75 ft N.
 Bank of creek at toe of W. ft at Dam site
 Creek bot. at Dam site
 E. End Dam site
 on knoll in Valley 600 ± N. of So. Prop line
 Surface Grd. near E. line + 200 ± So. of RD
 Creek bot " " " " " " " "

144

83.57
96.50
6x98

83.57
429
7928

100.4
11344

172
49
172

90.06
97.10
92.90
90.06
83.50

44.5656
2.60

1.96
11.74
97.80
13.94

495

83.57
899.50
4.07

357

5
7.07

1.72
1000
860
2940

172
48.00
344

1360
1204
90.06
80.90

93.06
456

88.50
10493
88.70

16.23
260
13.63
260

11.02
130
9.73
1.29

83.57
3.92
70.65
76.00

83.57
3.65
76.50

557
48
2456
2228
27736

76.28
83.57
76.28
7x29
429

78.3
83.5
161.8
80.9

95.2 13
5.94
130
464

83.57
79
83.57
4.10
79x47

146

{Center
Hambden}
ROAD

14

P.L. 20+46

⊙ 20+00 C.P.

P.L. 18+97

P.L. 18+36

Bone-
Orchard

Church
18+02
⊙ 18+00 C.P.

17+11

?

P.L. 15+93 ⊙ 16+00 C.P.

P.L. ? 15+08 culvert

Cobb

⊙ 14+00 C.P.
13+55 P.L.

road

Park

12+00 C.P.

Sta 11+33
Stn Chardon Thompson Road

147

(Twp. maps done) - Rex

HAMB DEN

148

Sta: 11+33 Φ E/W Rd.

0 10+00

P.L. 9+16

P.L. 8+36

P.L. 7+72 0 8+00 C.P.

P.L. 7+56 - - - - -

P.L. Ditch 6+96

[H]

[+]

P.L. 6+19

6+10 P.L.

4+85

0 5+00

4+79

T.B.V. Co.

HAMB DEN



0 4+00 C.P.

King

1+78

Riverside

0 0+00 C.P.

Φ

Φ

149

26+03 P.L.

Sta 26+00

25+56 P.L.

Chamberlain

24+16 P.L.

Sta 24+00 C.P.

St. John

22+95 P.L.

Carver

Sta 22+00 C.P.

20+69 P.L.

King

Old Cutts
place (now
King)

Sta 20+00 C.P.

P.L. 19+62

(Dope for
Township
maps)



HAMB DEN

150

P.L. 19+26

19+34 P.L.

Lewis

Emery Stone

C.P. 18+00

Sta 17+57

17+74

~~Lewis~~

Sta 17+49

Kirby

House Whitney Store
C.P. 16+00

X pt
Sta 15+76

P.L. Sta. 15+41

PARK

Sta 14+64

C.P. 14+00
PARK

P.L. Sta. 13+56

I

Plow Line 12+10

Barn
C.P. 12+00

P.L. 11+80

Plow Line? Sta 11+40?

church

P.L. 10+00

P.L. 10+00

P.L. Sta. 10+70

I

PL Sta 9+75

I

Grange Hall

P.L. 9+84

8+93

Sta 9+00

School

Sta 9+34 P.L. 157

P.L. Sta 8+93

1101.3

12.8
1088.5

School

Sta 8+02 - P.L.

Sta 8+00 C.P. (Culvert)

Orchard

Sta 6+75

I

Town Hall

600 C.P.

Sta 5+50+

B

Sta 5+10 P.L. - Brush Line

Sta 4+00 C.P.

Nemas

P.L. Sta 2+56

A

542+00 C.P.

Sta. 194

EDLINCKI

Sta 15+4

Stands

Sta. 6+00 - W. Edge of Road

152
①

~~Battles Road~~

HAMBDEN W

Weston

178.4'

B. HOUSE

113'

Russell

410'

N. of
prop.

264.00
N. LINE
E.M. Stone

H

247'

Thompson

to Edge of
194'

to Corners
Chardon

131'

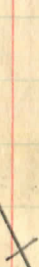
P.L.

329'

H

B

P.L.



75.65
74.35
1.30

234
128
362
2320
472
7582
1438
795
513

155
47
560
7582
1438
795
513

65
236
130
170
200
165
20.5
7482
4.69
45
15
29
450
155
310
400
1395
129
55
745
145
1595
145

145
95
79.15
75.69
381
3.145

129
75.55
95.84
3.67
14
3.67
381

351
95.55
245
75.69

70.5
75.70
32
3

79.57
3.88
25.84

134
15840
2160

TABLE IX.—CALCULATION OF EARTHWORK.

Width	HEIGHT														
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
1	.02	.04	.06	.07	.09	.11	.13	.15	.17	.18	.20	.22	.24	.26	.28
2	.04	.07	.11	.15	.18	.22	.26	.30	.33	.37	.41	.44	.48	.52	.56
3	.06	.11	.17	.22	.28	.33	.39	.44	.50	.56	.61	.67	.72	.78	.83
4	.07	.15	.22	.30	.37	.44	.52	.59	.67	.74	.81	.89	.96	1.04	1.11
5	.09	.19	.28	.37	.46	.56	.65	.74	.83	.93	1.02	1.11	1.20	1.30	1.39
6	.11	.22	.33	.44	.56	.67	.78	.89	1.00	1.11	1.22	1.33	1.44	1.55	1.67
7	.13	.26	.39	.52	.65	.78	.91	1.04	1.16	1.30	1.42	1.55	1.68	1.81	1.94
8	.15	.30	.44	.59	.74	.89	1.04	1.19	1.33	1.48	1.63	1.78	1.92	2.08	2.22
9	.17	.33	.50	.67	.83	1.00	1.17	1.33	1.50	1.67	1.83	2.00	2.17	2.33	2.50
10	.18	.37	.56	.74	.93	1.11	1.30	1.48	1.67	1.85	2.04	2.22	2.41	2.59	2.78
11	.20	.41	.61	.82	1.02	1.22	1.43	1.63	1.83	2.04	2.24	2.44	2.65	2.85	3.06
12	.22	.44	.67	.89	1.11	1.33	1.56	1.78	2.00	2.22	2.44	2.67	2.89	3.11	3.33
13	.24	.48	.72	.96	1.20	1.44	1.68	1.92	2.16	2.41	2.65	2.89	3.13	3.37	3.61
14	.26	.52	.78	1.04	1.30	1.55	1.81	2.08	2.33	2.59	2.85	3.11	3.37	3.63	3.89
15	.28	.56	.83	1.11	1.39	1.67	1.94	2.22	2.50	2.78	3.06	3.33	3.61	3.89	4.17
16	.30	.59	.89	1.18	1.48	1.78	2.07	2.37	2.67	2.96	3.26	3.56	3.85	4.15	4.44
17	.31	.63	.94	1.26	1.57	1.89	2.20	2.52	2.83	3.15	3.46	3.78	4.09	4.41	4.72
18	.33	.67	1.00	1.33	1.67	2.00	2.33	2.67	3.00	3.33	3.67	4.00	4.33	4.67	5.00
19	.35	.70	1.06	1.41	1.76	2.11	2.46	2.82	3.17	3.52	3.87	4.22	4.57	4.92	5.28
20	.37	.74	1.11	1.48	1.85	2.22	2.59	2.96	3.33	3.70	4.07	4.44	4.81	5.18	5.56
21	.39	.78	1.17	1.55	1.94	2.33	2.72	3.11	3.50	3.89	4.28	4.67	5.06	5.44	5.83
22	.41	.81	1.22	1.63	2.04	2.44	2.85	3.26	3.67	4.07	4.48	4.89	5.30	5.70	6.11
23	.43	.85	1.28	1.70	2.13	2.56	2.98	3.41	3.83	4.26	4.68	5.11	5.54	5.96	6.39
24	.44	.89	1.33	1.78	2.22	2.67	3.11	3.56	4.00	4.44	4.89	5.33	5.78	6.22	6.67
25	.46	.92	1.39	1.85	2.31	2.78	3.24	3.70	4.17	4.63	5.09	5.56	6.02	6.48	6.94
26	.48	.96	1.44	1.92	2.41	2.89	3.37	3.85	4.33	4.82	5.30	5.78	6.26	6.74	7.24
27	.50	1.00	1.50	2.00	2.50	3.00	3.50	4.00	4.50	5.00	5.50	6.00	6.50	7.00	7.50
28	.52	1.04	1.55	2.07	2.59	3.11	3.63	4.15	4.67	5.18	5.70	6.22	6.74	7.26	7.78
29	.54	1.07	1.61	2.15	2.68	3.22	3.76	4.30	4.83	5.37	5.91	6.44	6.98	7.52	8.06
30	.56	1.11	1.67	2.22	2.78	3.33	3.89	4.44	5.00	5.55	6.11	6.67	7.22	7.78	8.33
31	.57	1.15	1.72	2.30	2.87	3.44	4.02	4.59	5.17	5.74	6.32	6.89	7.46	8.04	8.61
32	.59	1.18	1.78	2.37	2.96	3.56	4.15	4.74	5.33	5.92	6.52	7.11	7.70	8.30	8.89
33	.61	1.22	1.83	2.44	3.05	3.67	4.28	4.89	5.50	6.11	6.72	7.33	7.94	8.55	9.17
34	.63	1.26	1.89	2.52	3.15	3.78	4.40	5.04	5.67	6.29	6.93	7.56	8.18	8.81	9.44
35	.65	1.30	1.94	2.59	3.24	3.89	4.53	5.18	5.83	6.48	7.13	7.78	8.42	9.08	9.72
36	.67	1.33	2.00	2.67	3.33	4.00	4.66	5.33	6.00	6.67	7.33	8.00	8.67	9.33	10.00
37	.68	1.37	2.06	2.74	3.42	4.11	4.79	5.48	6.17	6.85	7.54	8.22	8.91	9.59	10.28
38	.70	1.41	2.11	2.82	3.52	4.22	4.92	5.63	6.33	7.03	7.74	8.44	9.15	9.85	10.56
39	.72	1.44	2.17	2.89	3.61	4.33	5.05	5.78	6.50	7.22	7.95	8.67	9.39	10.11	10.83
40	.74	1.48	2.22	2.96	3.70	4.44	5.18	5.92	6.67	7.41	8.15	8.89	9.63	10.37	11.11

Table gives cu. yds. in 1 ft. of a triangle of given width and height. Corrections for tenths of width are one tenth the values found under each height considering the widths from 1 to 9 as tenths and similarly the corrections for tenths of height are one tenth the figures opposite width considering the heights from 1 to 9 as tenths. Thus if $w = 16.2$ and $h = 5.3$, cu. yds. $= 1.48 + .028 + .089 = 1.597$ cu. yds. or practically 160 cu. yds. per 100 ft. If w exceeds 40 ft., use one half and multiply result by 2, if both w and h are large use one half of each and multiply result by 4. Any cross-section may be divided into triangles by the following rule. To the triangle of the sum of the outside cuts (or fills) $= h$, and $\frac{1}{2}$ the roadbed $= w$, add the triangles formed by taking the distance out to each break in turn ($= w$'s) by the difference between the cuts (or fills) on each side of it ($= h$'s) always subtracting the outer from the inner.

DISTANCES FROM CENTER OF ROADWAY FOR CROSS-SECTIONING.

Roadway 16 feet wide. Side Slopes 1 on 1½.
For Single Track Embankment.

H	0	.1	.2	.3	.4	.5	.6	.7	.8	.9	H
0	8.0	8.2	8.3	8.5	8.6	8.8	8.9	9.1	9.2	9.4	0
1	9.5	9.7	9.8	10.0	10.1	10.3	10.4	10.6	10.7	10.9	1
2	11.0	11.2	11.3	11.5	11.6	11.8	11.9	12.1	12.2	12.4	2
3	12.5	12.7	12.8	13.0	13.1	13.3	13.4	13.6	13.7	13.9	3
4	14.0	14.2	14.3	14.5	14.6	14.8	14.9	15.1	15.2	15.4	4
5	15.5	15.7	15.8	16.0	16.1	16.3	16.4	16.6	16.7	16.9	5
6	17.0	17.2	17.3	17.5	17.6	17.8	17.9	18.1	18.2	18.4	6
7	18.5	18.7	18.8	19.0	19.1	19.3	19.4	19.6	19.7	19.9	7
8	20.0	20.2	20.3	20.5	20.6	20.8	20.9	21.1	21.2	21.4	8
9	21.5	21.7	21.8	22.0	22.1	22.3	22.4	22.6	22.7	22.9	9
10	23.0	23.2	23.3	23.5	23.6	23.8	23.9	24.1	24.2	24.4	10
11	24.5	24.7	24.8	25.0	25.1	25.3	25.4	25.6	25.7	25.9	11
12	26.0	26.2	26.3	26.5	26.6	26.8	26.9	27.1	27.2	27.4	12
13	27.5	27.7	27.8	28.0	28.1	28.3	28.4	28.6	28.7	28.9	13
14	29.0	29.2	29.3	29.5	29.6	29.8	29.9	30.1	30.2	30.4	14
15	30.5	30.7	30.8	31.0	31.1	31.3	31.4	31.6	31.7	31.9	15
16	32.0	32.2	32.3	32.5	32.6	32.8	32.9	33.1	33.2	33.4	16
17	33.5	33.7	33.8	34.0	34.1	34.3	34.4	34.6	34.7	34.9	17
18	35.0	35.2	35.3	35.5	35.6	35.8	35.9	36.1	36.2	36.4	18
19	36.5	36.7	36.8	37.0	37.1	37.3	37.4	37.6	37.7	37.9	19
20	38.0	38.2	38.3	38.5	38.6	38.8	38.9	39.1	39.2	39.4	20
21	39.5	39.7	39.8	40.0	40.1	40.3	40.4	40.6	40.7	40.9	21
22	41.0	41.2	41.3	41.5	41.6	41.8	41.9	42.1	42.2	42.4	22
23	42.5	42.7	42.8	43.0	43.1	43.3	43.4	43.6	43.7	43.9	23
24	44.0	44.2	44.3	44.5	44.6	44.8	44.9	45.1	45.2	45.4	24
25	45.5	45.7	45.8	46.0	46.1	46.3	46.4	46.6	46.7	46.9	25
26	47.0	47.2	47.3	47.5	47.6	47.8	47.9	48.1	48.2	48.4	26
27	48.5	48.7	48.8	49.0	49.1	49.3	49.4	49.6	49.7	49.9	27
28	50.0	50.2	50.3	50.5	50.6	50.8	50.9	51.1	51.2	51.4	28
29	51.5	51.7	51.8	52.0	52.1	52.3	52.4	52.6	52.7	52.9	29
30	53.0	53.2	53.3	53.5	53.6	53.8	53.9	54.1	54.2	54.4	30
31	54.5	54.7	54.8	55.0	55.1	55.3	55.4	55.6	55.7	55.9	31
32	56.0	56.2	56.3	56.5	56.6	56.8	56.9	57.1	57.2	57.4	32
33	57.5	57.7	57.8	58.0	58.1	58.3	58.4	58.6	58.7	58.9	33
34	59.0	59.2	59.3	59.5	59.6	59.8	59.9	60.1	60.2	60.4	34
35	60.5	60.7	60.8	61.0	61.1	61.3	61.4	61.6	61.7	61.9	35
36	62.0	62.2	62.3	62.5	62.6	62.8	62.9	63.1	63.2	63.4	36
37	63.5	63.7	63.8	64.0	64.1	64.3	64.4	64.6	64.7	64.9	37
38	65.0	65.2	65.3	65.5	65.6	65.8	65.9	66.1	66.2	66.4	38
39	66.5	66.7	66.8	67.0	67.1	67.3	67.4	67.6	67.7	67.9	39
40	68.0	68.2	68.3	68.5	68.6	68.8	68.9	69.1	69.2	69.4	40

Example—If point is 22.6 ft. above grade, how far should it be from center line to be a slope stake point? Ans. from Table 41.9. For same slopes but other widths of roadbed correct above figures by one-half difference in width of roadbed; thus in example above for 20 ft. roadbed distance will be $41.9 + (20 - 16) \div 2$ or 2 ft. added to 41.9 = 43.9. For slopes of 1 on 1 see inside of front cover.

